

# New Models and Features in ATHLET 3.5

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Philipp Schöffel, GRS

AC<sup>2</sup> User Meeting, GRS Köln, 18.11.2025

# Content

- **New and Updated Models in ATHLET 3.5**
  - New models for **structures and internals**
    - Spacer grid modelling
    - Geometry, materials and heat conduction in HCOs
  - Extended **Flow Regime Maps and Friction Loss Models**
  - Component Model Updates: **Heat Pipe, Critical Discharge**
- **Input, Output and Postprocessing**
  - 3D TFO and HCO data
  - New Input Options and Output Data
- **Summary**

# Modelling of Rod Bundles with Spacer Grids

**Objective:** Capture spacer grid effects on **TH behavior during core uncover**

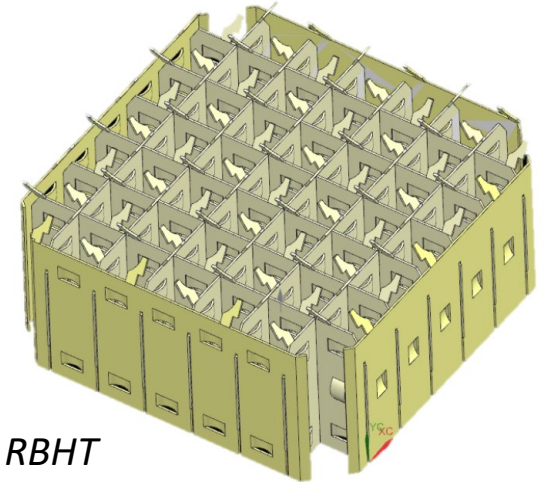
- **Convective heat transfer enhancement** downstream the spacer grid
- Increase of interfacial area and interfacial transfers due to **droplet breakup**

Previous ATHLET spacer grid model only considered impact on CHF

- Applicable with **Groeneveld LUT**

$$q_{CHF,spacer} = \left[ 1 + A \exp \left( \frac{-B L_S}{D_H} \right) \right] q_{LUT}$$

- Requires provision of input data under
  - PW SPACER (HECU) defining positions of spacer grids
  - PW FRICTION (TFD) with mandatory zeta value for each spacer grid junction



*RBHT  
mixing vane  
spacer grid*

```

C---- HEATCOND
K---- HEATRIN
. . .
----- SPACER
@ SHSPAC0 (1...N)
  0.102   0.690   1.212 . . .
  
```

# Extended Spacer Grid Model

- Turbulence-induced **convective heat transfer enhancement** downstream the spacer grid

- Model options depend on **blockage ratio  $\varepsilon$**  or **friction loss  $K_g$**

- Yao:  $Nu_{\text{spacer}} = (1 + 5.55\varepsilon^2 e^{-0.13(L_s/d_h)}) \cdot Nu_0$

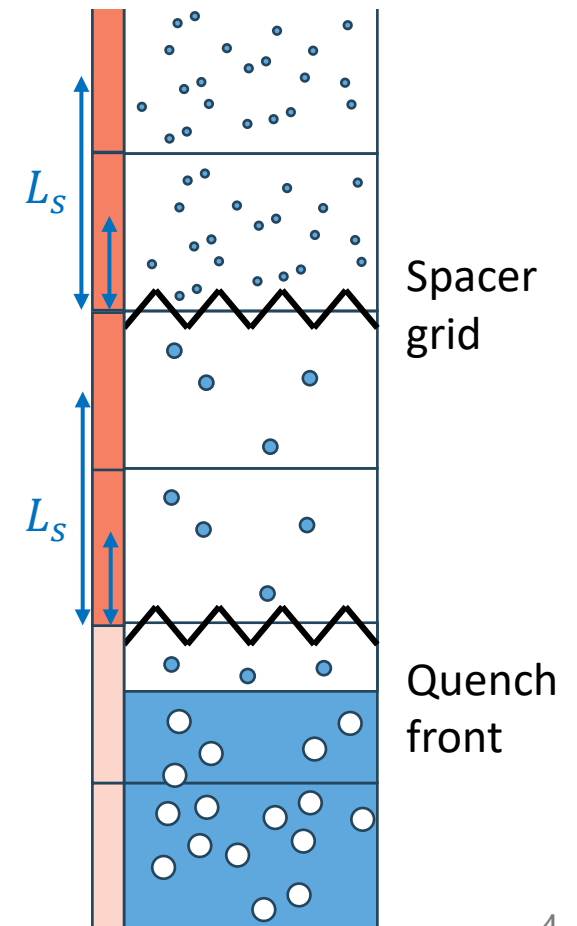
- Holloway:  $Nu_{\text{spacer}} = [1 + (0.8K_g - 0.4)e^{-0.25(L_s/d_h)}] \cdot Nu_0$

- Increase of interfacial area due to **droplet breakup**

- Reduced droplet Sauter mean diameter** downstream the grid, considered by evaporation model

$$\frac{d_{32}}{d_0} = 6.167 \cdot We^{-0.53}$$

- Applied for dispersed flow regime
- Considers quench front progression (if model is active)

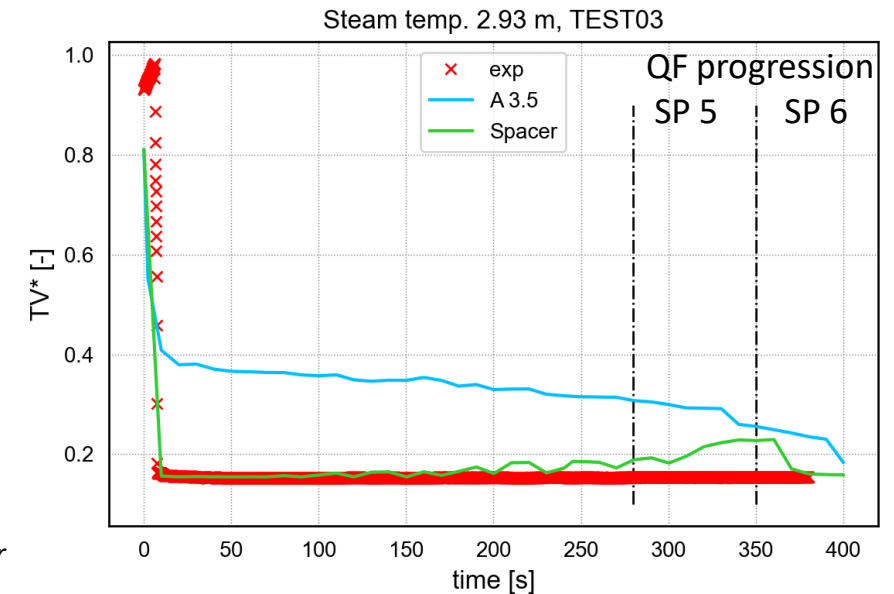
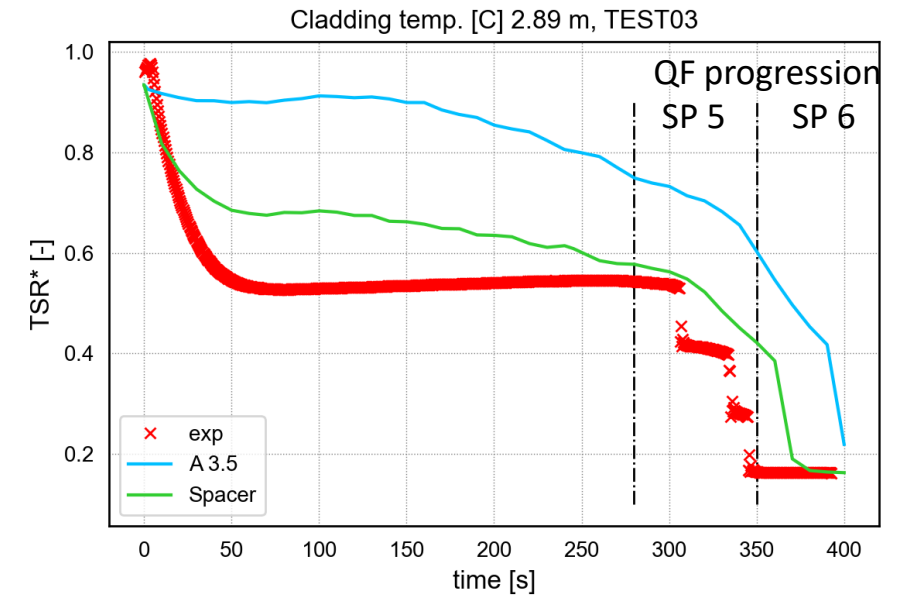
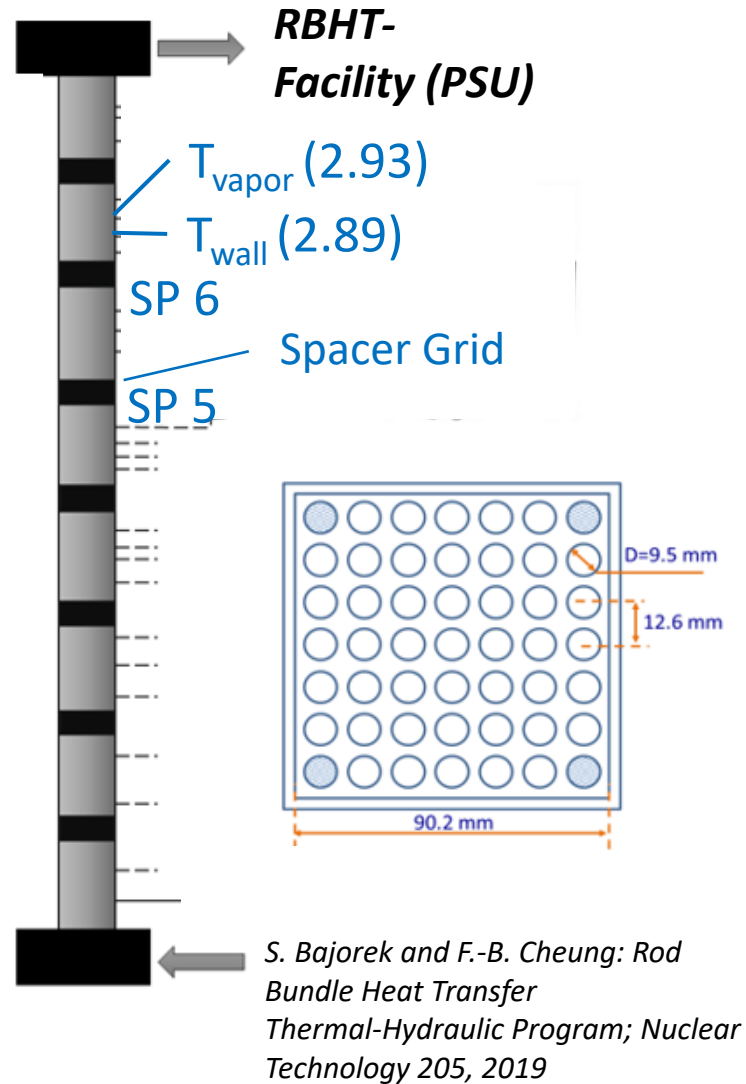


# Validation against RBHT Experiment

## OECD RBHT project

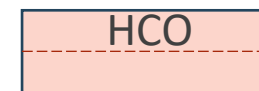
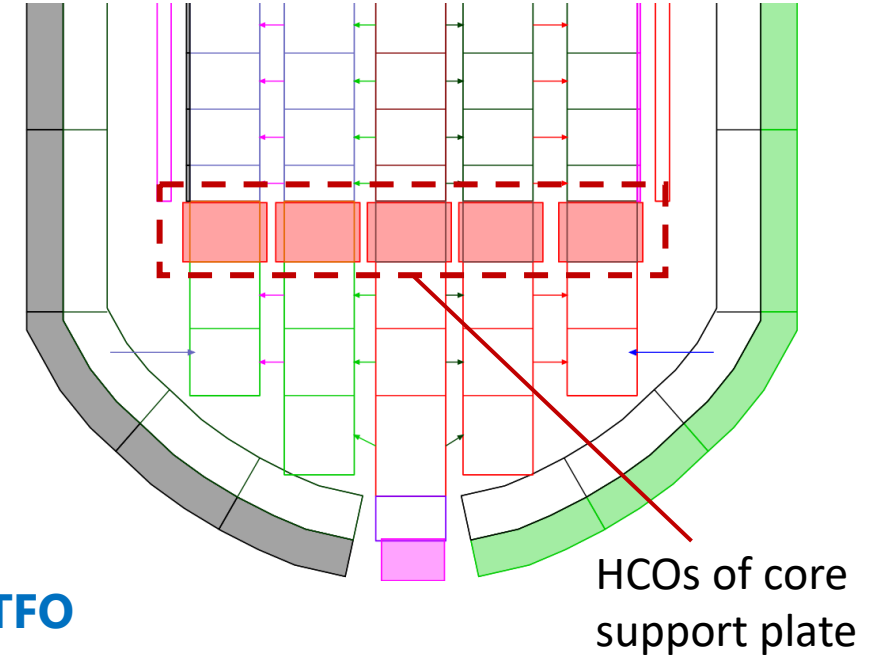
- Reflooding tests
- Pressure: 1 to 4 bar
- Subcooling: 3 to 80 K

## Cladding precooling downstream of the spacer grid

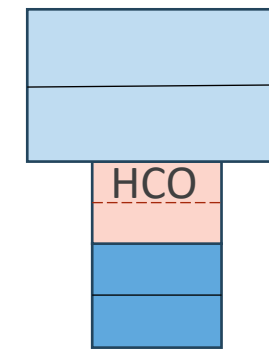


# Simulation of Horizontal Structures

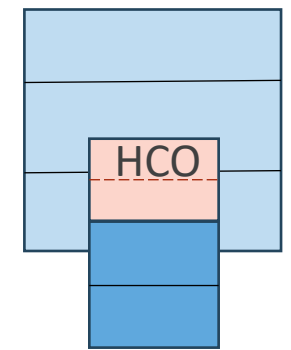
- Vessels or pools represented by vertically oriented TFOs
  - Up to now, coupling of an HCO only along axial direction of the corresponding TFO
  - **Limited accuracy** to model e.g. vessel lid, pool bottom, or a tie plate
  - **Need to couple an HCO orthogonally to a vertical TFO**
- **New HCO type “horizontal plate”** introduced
  - enables to couple a strictly horizontal HCO orthogonally to a (strictly vertical) CV
  - always consists of a single HCV



*one-sided coupling*



*two-sided coupling*

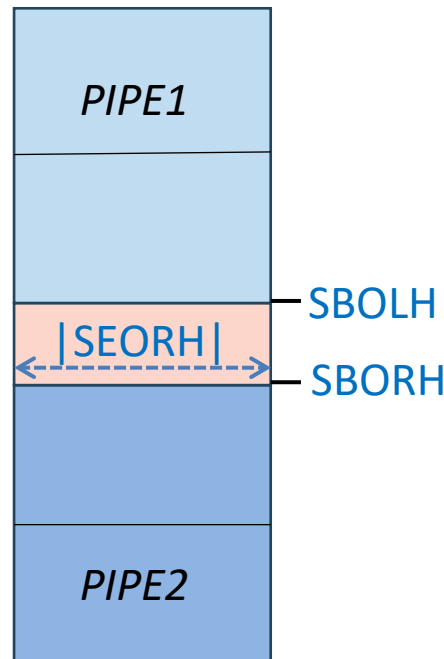


*coupling inside CV*

# Application of Horizontal Plate

```

K----- HORPLATE
@ AOLH  SBOLH SEOLH AORH  SBORH SEORH
  PIPE1    0.  -0.2 PIPE2    5.  -0.2
@ . . . IGEO0 ...
  . . .    0 ...
----- GEOMETRY
...
@ SG0  Z0  DI0  DS10 GAP10 ...
  0.    1.3 0.15 0.05 0.    ...
  0.2   1.3 0.15 0.05 0.    ...
  
```



- **By convention, the left side is the upper side**, the right side the lower side
- Coupling location inside the TFO is determined by SBOLH resp. SBORH
- A negative input value for SEOLH or SEORH indicates horizontal coupling. Its absolute value must be equal the length of the plate.

- Horizontal plate during application:
  - **Churchill correlation** for natural convection heat transfer at top and bottom side:
  - No specific correlations in other heat transfer regimes

$$Nu = c \cdot \left[ Ra \cdot \left[ 1 + \left( \frac{d}{Pr} \right)^a \right]^{-1/a} \right]^b$$

# New Options for Structure Materials

- HCOs may optionally consist of **more than three material zones**
  - Input parameter NADDMZ:**  
number of additional zones
  - Extension of further PWs where relevant, e.g. GEOMETRY, HTCDEF, MATPROP

```

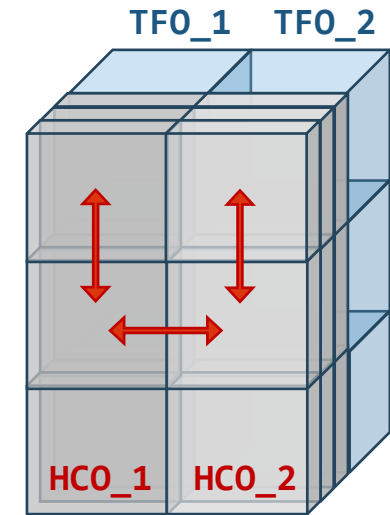
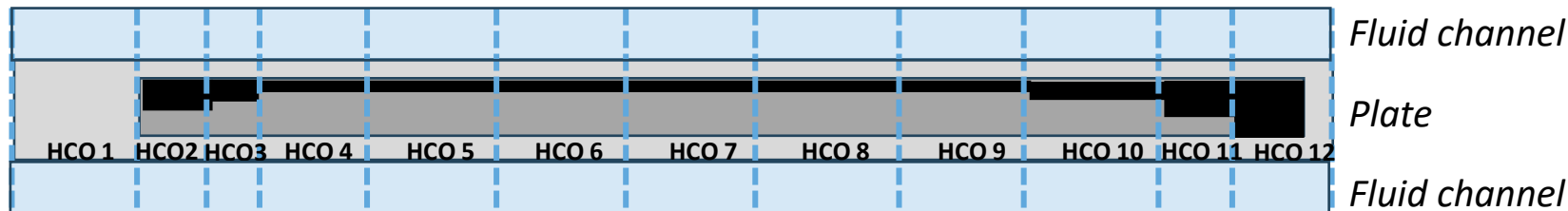
K----- H_BOILER    @ split into 6 material zones
@  AOLH            SBOLH  SEOLH   AORH            SBORH  SEORH
   ADIABAT         0.      0.      BOILER         0.02   0.07
@  NIHC0 N10 N20 N30 IGE00 ICOMP0 ACOMP0   ICHF0 NADDMZ
   1      10  2   2   5      0      DUMMY     2      3
@  N40  N50  N60
   2    2    2
@
----- GEOMETRY
. . .
----- HTCDEF
  
```

- Additional built-in materials available: **BORCARBIDE, INCONEL600, ALUMINA** ( $\text{Al}_2\text{O}_3$ )



# Simulation of 3D Heat Conduction in Structures

- **Motivation:** Detailed simulation of complex structural components
  - Usage of a 3D TFD network requires refining the HCO network
  - So far, HECU solved for a 1D or a pseudo-2D heat conduction equation
- **New CW HCOCONNECT** enables **3D heat conduction** by coupling of HCOs
  - Prerequisite: equal axial nodalization and equal number of layers
  - Alternative sparse matrix solver from PETSc package
- **Application:** plate-type fuel elements in research reactor \*



```

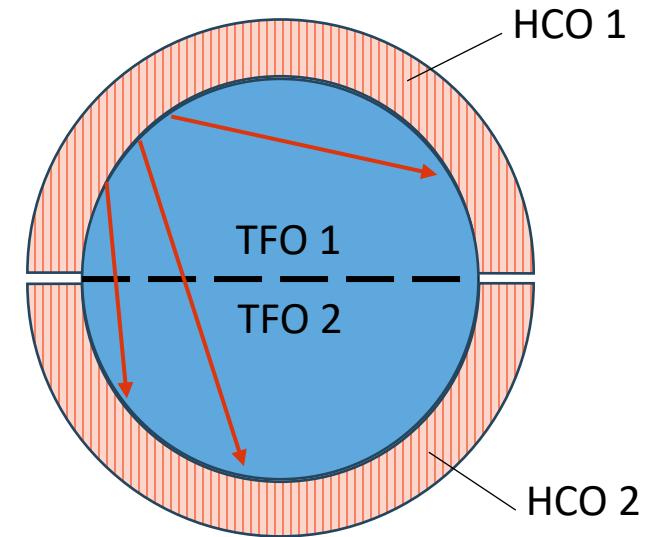
C----- HCOCONNECT
@  IHCSYS
   4
K----- Group1
. . . .
@  AHCOLIST(1,...,n)
   HCO_1  HCO_2  ...
  
```

\* See presentation by F. Weyermann

# Extended Thermal Radiation Model

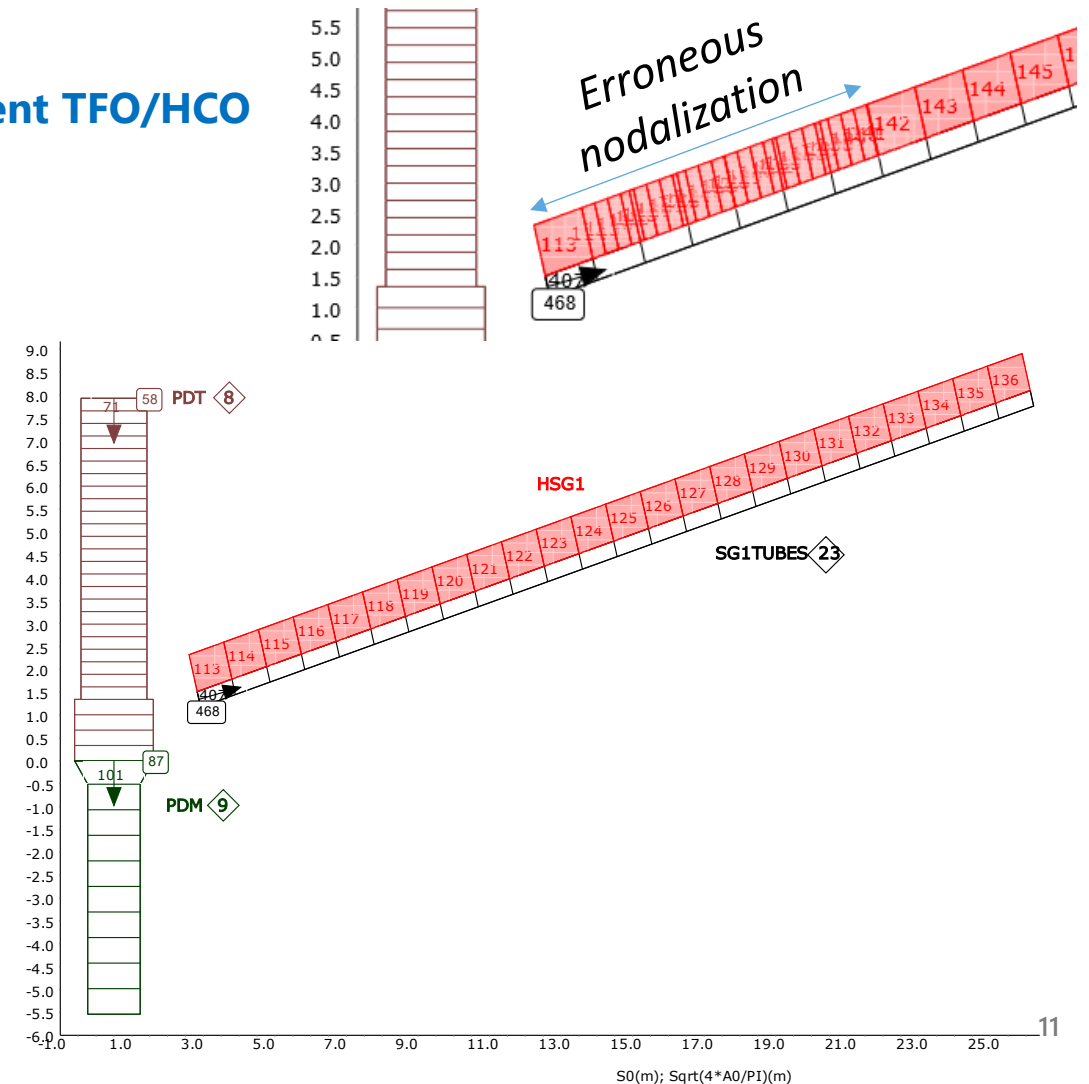
**Thermal radiation** between HCOs connected to *different* TFOs

- Definition of radiation group under **new KW FLEXRAD**
- All grouped HCOs must have the same length
- Optional shape factor  $s$  for energy flux:  $E = s \cdot \epsilon \cdot \sigma \cdot T^4$
- **Additional input check** to ensure reciprocity:  $A_1 \cdot \varphi_{1 \rightarrow 2} = A_2 \cdot \varphi_{2 \rightarrow 1}$



# Improvements of HECU Module for Helically Coiled HTEX

- Inside helical heat exchanger tube, **HTC calculation under film boiling conditions** uses Mc Eligot correlation (avoids program error)
- Improved automatic **HCO nodalization for non-congruent TFO/HCO**
  - Helical coil represented by inclined pipe
  - Erroneous HCO nodalization results caused program stop
    - Depending on orientation of inner and outer side TFOs
    - Work around: introduce numerous HCOs each consisting of one HCV
  - Improved program implementation provides HCO **nodalization that matches both adjacent TFOs**
  - Increased user friendliness**



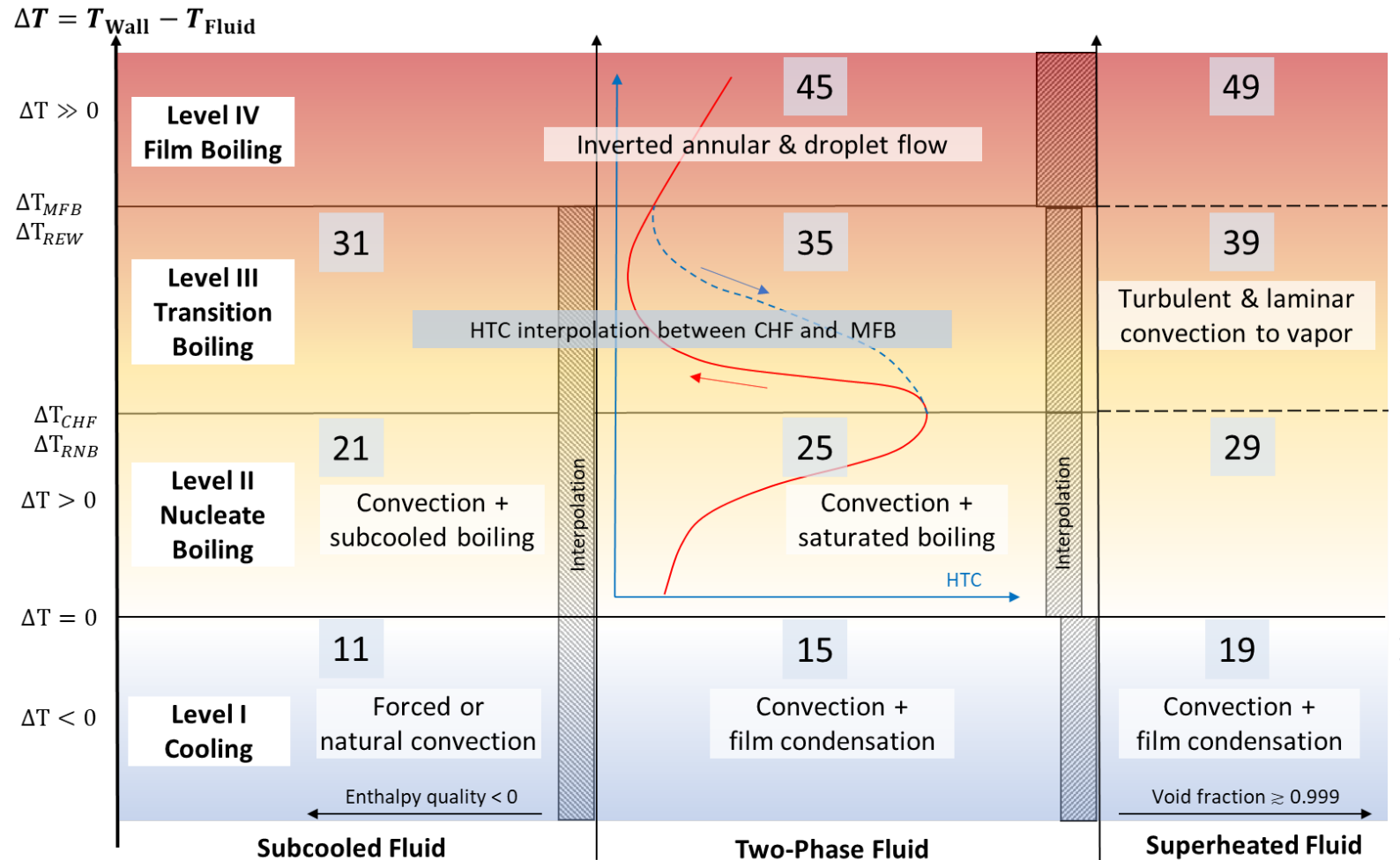
# Extended Plug-ins for User-provided HTC and CHF Correlations

## MHTCEXT plug-in

- Comprises set of interfaces for various heat transfer regimes and working fluids
- New interface** for convective heat transfer to vapor in **DFFB regime (mode 49)**

## Extended CHF plug-in

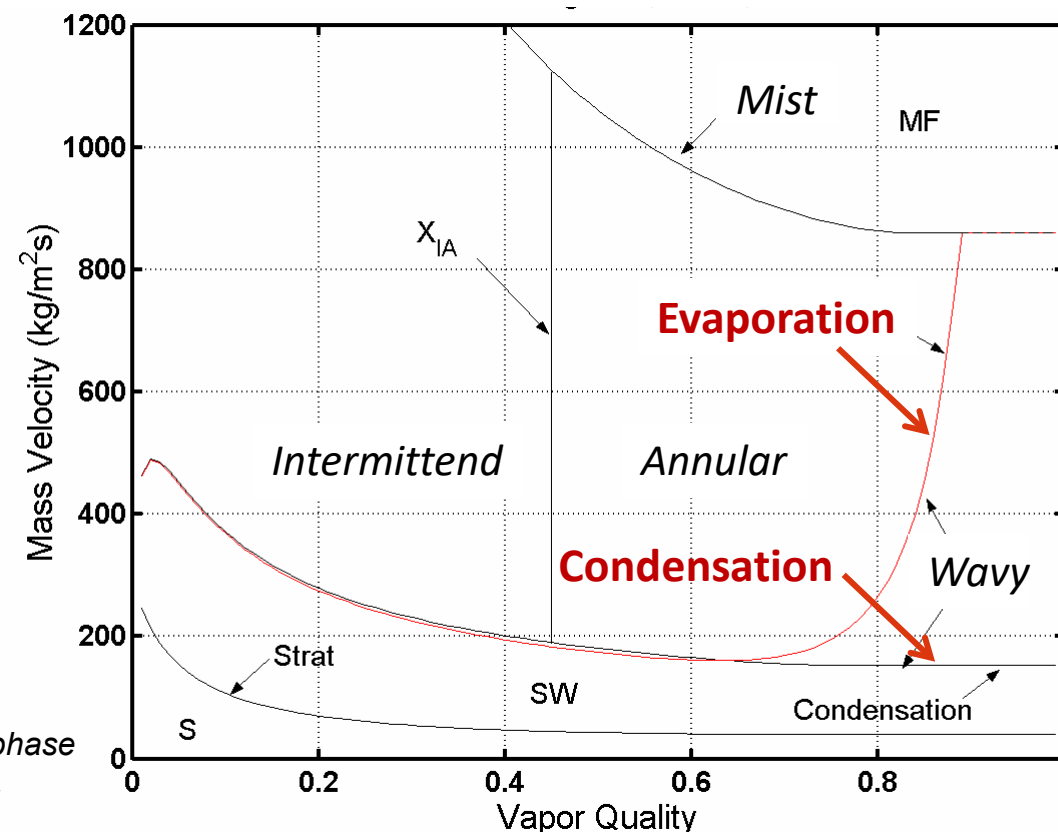
- Interface provides **access to TH quantities at core channel entry**
- OMP-safe access to ATHLET global variables** via plug-in function `execute_c`



# Unified and Extended Flow Regime Maps

- **Motivation:** Use of dedicated flow regime maps for both boiling as well as condensing flows
  - Centralized flow regime calculation (based on Taitel-Dukler) with **unified flow pattern map**
  - Unified calculation of the entrained liquid fraction
  - Output of current flow regime
- For **flows with wall condensation (passive systems)**
  - **Adjusted flow regime map** focusing on **horizontal annular flow**
- Steady transition between flow regime maps for  $-1\text{ °C} \leq T_{\text{wall}} - T_{\text{sat}} \leq 0\text{ °C}$
- Optional model, to be activated under CW MISCELLAN

\* Hajal, J. E., Thome, J. R., Cavallini, A.: Condensation in horizontal tubes, part 1: two-phase flow pattern map. *International Journal of Heat and Mass Transfer*, Bd. 46, Nr. 18, 2003.



# Closure Laws for Flow Regimes with Wall Condensation

- Dedicated closure laws for **annular flow and stratified/stratified wavy flow**

- Interfacial friction**

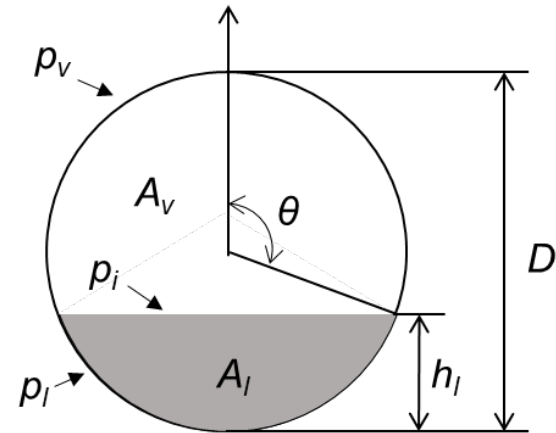
- $C_{i,str} = \frac{1}{2} \rho_v \lambda_v \frac{4 \sin \theta}{D_h \pi}$  (Taitel-Dukler)

- $C_{i,wavy} = \frac{1}{2} \rho_v \lambda_v \left( 1 + 15 \left( \frac{h_l}{D_h} \right)^{0.5} \left( \frac{j_v}{j_{v,crit}} - 1 \right) \right) \frac{4 \sin \theta}{D_h \pi}$  (Andritsos-Hanratty)

- $C_{i,ann} = \frac{1}{2} \rho_v 0.005 [1 + 75(1 - \alpha)] \frac{4}{D_h} \sqrt{\alpha}$  (Wallis)

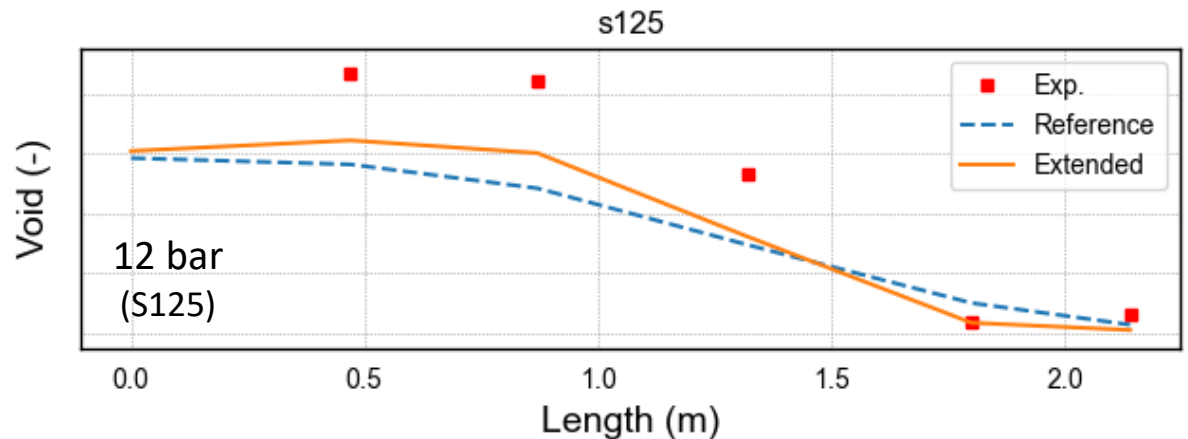
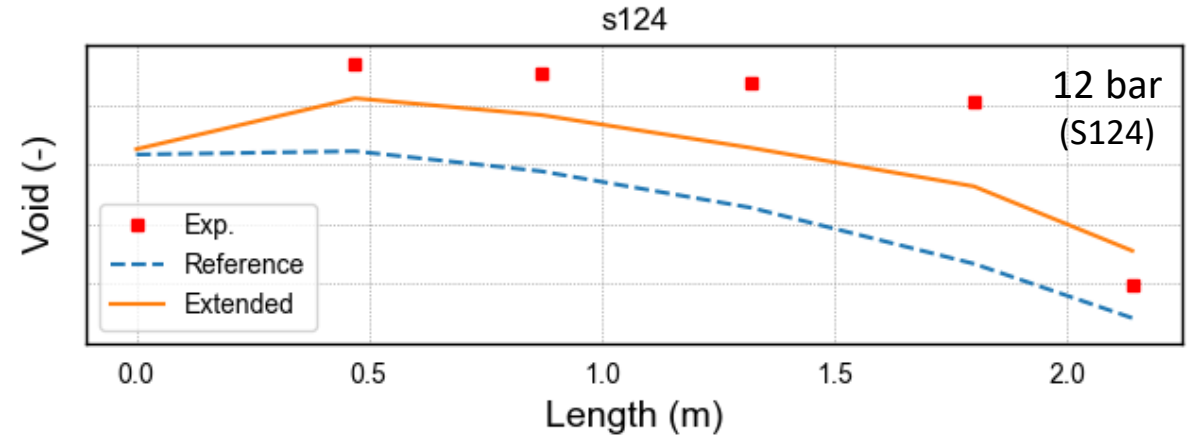
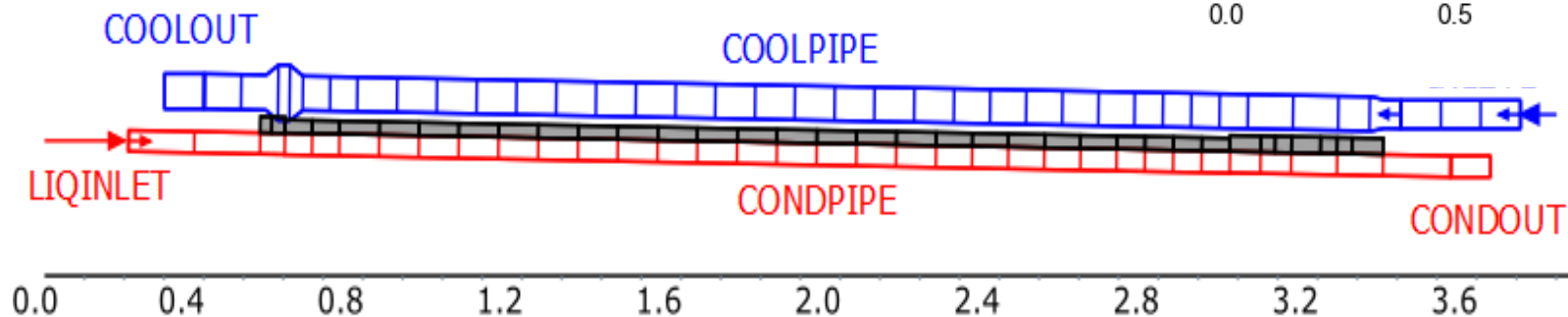
- Wall friction** distribution to phases according to dry / wetted perimeter

- Annular flow: wall friction completely assigned to liquid phase



# Validation of Flow Regime Map Module for Horizontal Pipe

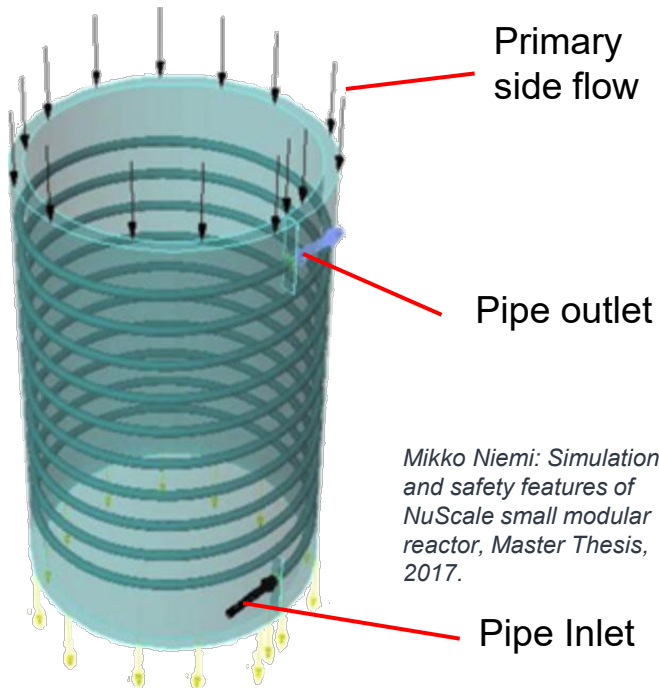
- **COSMEA experiment** with coaxial double pipe
- Slightly inclined pipe ( $L = 2.82$  m,  $D = 43$  mm)
- Condensation of steam in inner pipe
- On-going work related to
  - **Wall heat flow distribution** to phases
  - **Harmonization of wall condensation and bulk condensation models**



# Friction Loss for Special Components

## Cross flow in bundle (in-line or staggered arrangement)

- friction loss  **$\zeta$  dependent on Reynolds number**  $\zeta = \zeta_{\text{lam}} + \zeta_{\text{turb}} \cdot F(Re)$
- Dedicated correlation to be activated via CW FORMLOSS
- Automatically employed for helical heat exchanger (PW HTEXDEF)



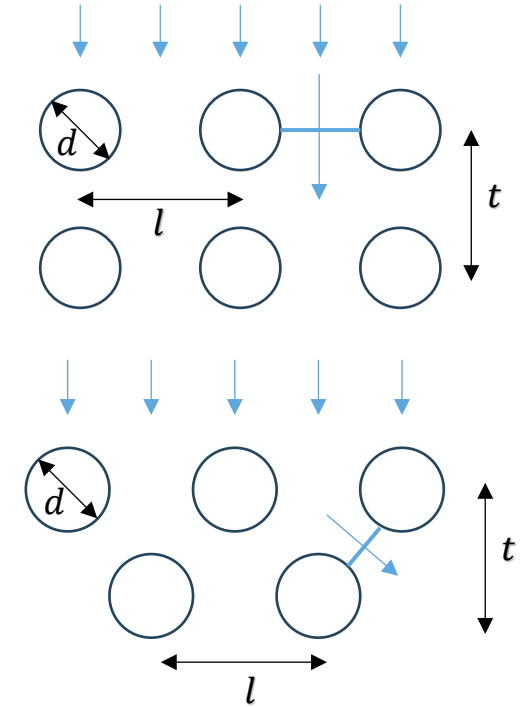
Mikko Niemi: Simulation and safety features of NuScale small modular reactor, Master Thesis, 2017.

## For helical heat exchanger (inner side)

- Modified friction factor \*:  $\lambda_{\text{helix}} = \lambda_{\text{turb}} \left( Re \left( \frac{d_h}{d_{\text{coil}}} \right)^2 \right)^{1/20}$
- 2-phase flow with modified Martinelli-Nelson multiplier  $\Phi_{tt}$
- Development by RUB/J. Krieger \*\*

\* Nariai et al.: Friction pressure drop and heat transfer coefficient of two-phase flow in helically coiled tube once-through steam generator, J. Nucl. Sic. Technol. 19, 1982

\*\* Krieger et al.: Simulation of the experiment OSU-002 regarding the behavior of a helically coiled steam generator using AC<sup>2</sup>-ATHLET, ICONES30, 2023



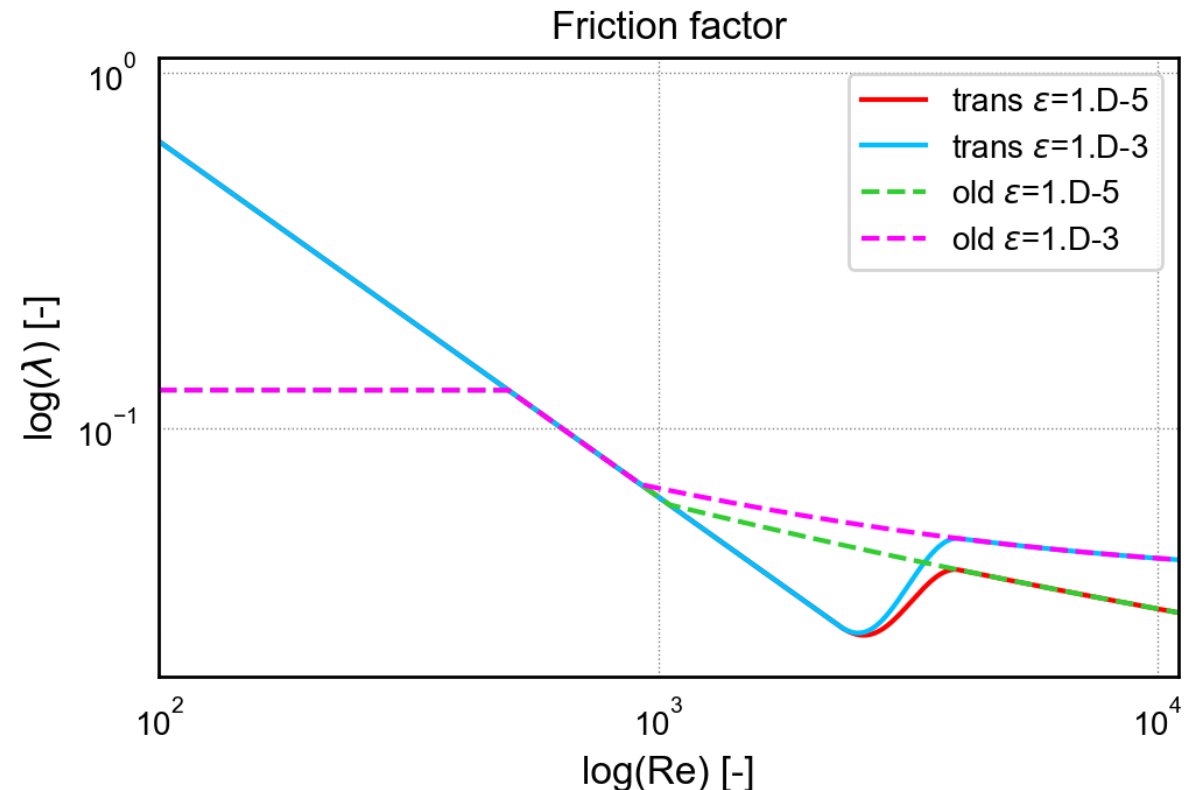


# Wall Friction in Laminar-turbulent Transition

**Motivation:** improved calculation of wall friction at **low Re-numbers** (IKE, M. Abd El Malek)

- **Start-up behavior of passive systems**
- So far, Darcy-Weisbach friction factor as maximum of Hagen-Poiseuille and Colebrook:  $\lambda = \max(\lambda_{\text{lam}}, \lambda_{\text{turb}})$
- **Improved model with cosine-shape transition** between  $\lambda_{\text{lam}}$  and  $\lambda_{\text{turb}}$  for  $2300 \leq Re \leq 4000$ 
  - For laminar flow: limitation of  $\lambda$  to  $Re_L \geq 5$
  - Default model for pipe and annulus geometry
  - Input parameter **ITRNS** to select friction model
  - Adjustable Reynolds **interpolation range**

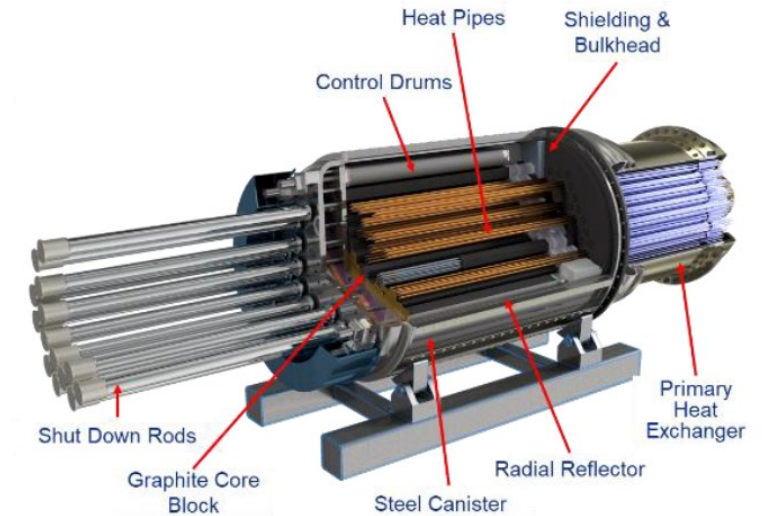
----- FRICTION			
@	ITPMO	ALAMO	ROUO
	2	1.0	1.D-5
@			
@	<b>ITRNS</b>	<b>TRNS1</b>	<b>TRNS2</b>
	1	2000.	3000.



# New Feature: High-Temperature Heat Pipe Module

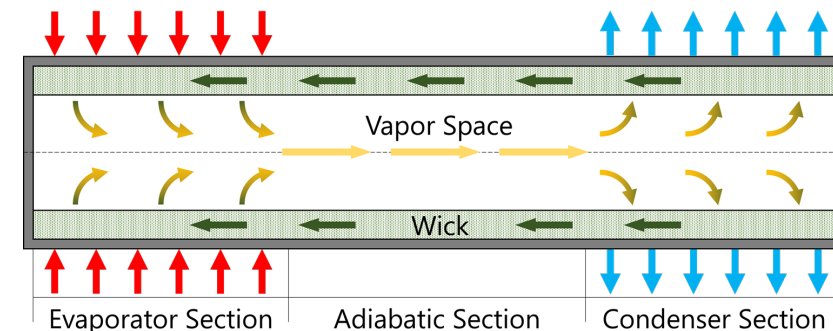
- **Liquid metal heat pipe-cooled MMR** (eVinci, SPR, ...)
- Development of ATHLET for MMR safety analysis
- ATHLET Heat Pipe Module comes with **specific models** \*
  - **Wick structure, capillary pumping, phase change, friction loss**
  - Covers **different wick types** and materials
  - Working fluids: Sodium, Potassium
  - Works with NC gases
  - For horizontal and vertical heat pipes

\* Details in presentation by D. Eckert



## eVinci reactor system overview

Hong Xu, Yizhou Yan, Oriol Noguera Oliva, "CFD Thermal Analysis for Primary Heat Exchanger of eVinci™ Nuclear Test Reactor", 21th International Topical Meeting on Nuclear Reactor Thermal Hydraulics, Busan, South Korea, August 31<sup>th</sup> - September 5<sup>th</sup> 2025



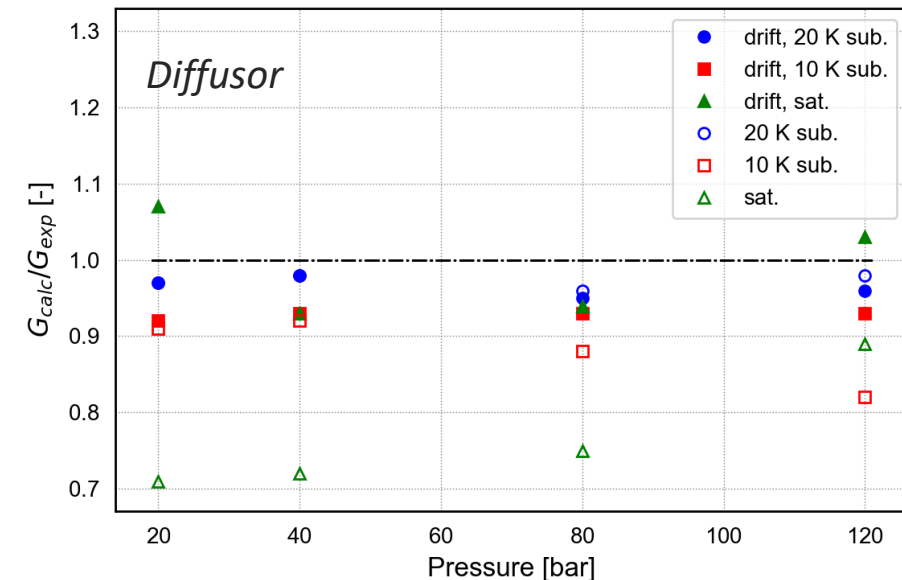
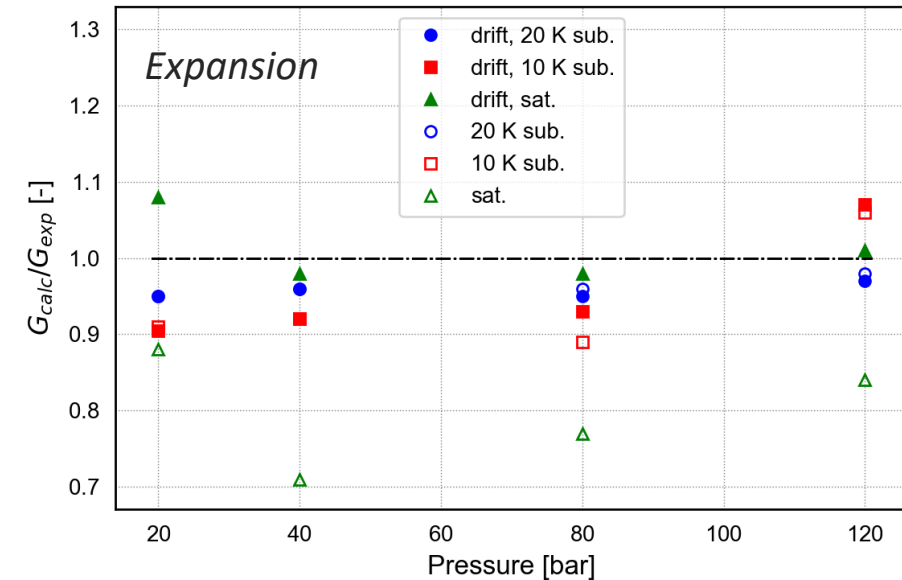
# New Option for Critical Discharge Rate Calculation

## Critical discharge model CDR1D extended by optional consideration of phase drift

- 4-eq. system with phase slip

$$S = 1 + \frac{3}{2} \sqrt{3\alpha} (1 - \alpha) \left( \left( \frac{\rho_l}{\rho_v} \right)^{1/3} - 1 \right)$$

- Application of ATHLET standard evaporation model:
  - Input parameter **TURB defines bubble number density**
- Activated under CW DISCHARGE: IAUR=5
- Validation against Super Moby Dick experiment
  - 20 mm nozzle
  - Two different geometries investigated: Sudden expansion or diffuser
- Further model validation required



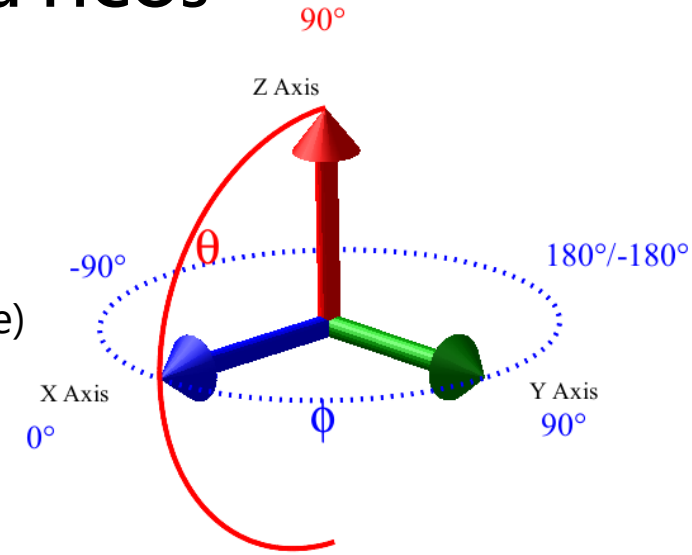
# Integration of ATHLET-CD

- **Ongoing ATHLET-CD integration into ATHLET** makes several modules available \*
  - VENTINA for initial inventory calculation and decay of isotopes
  - FPREL and SAFT for release, transport and deposition of radionuclides in LWR
  - THEMEC for fuel rod behavior, ballooning, and feedback on thermal-hydraulics (blockage)
  - Enables accident simulation without core degradation/until melting

*\* Details in presentation by L. Lovasz*

# New Input and Output Options: 3D Data for TFOs and HCOs

- **Motivation:** Extend ATHLET by 3D information
  - Compact 3D graphical system representation
  - Future usage of 3D data by physical models (e.g. thermal radiation in 3D core)
- **Basic geometry information** derived from CW TOPOLOGY
- Additional 3D data from **optional extension of PW GEOMETRY**
  - **rotation angle  $\Phi$  in XY plane**
- Optional input under **new PW POSITION**
  - Rotation angle and (x,y,z) coordinate at TFO origin
  - Parameters to define if data are absolute or relative to preceeding TFO
  - Positioning of first TFO of each TFD system
  - Easy copying of TFOs with different spatial orientation
  - Note: changes in height position influence TH simulation



```

C----- OBJECT
. . .
----- GEOMETRY
@ SG0    Z0    D0    A0    V0    DEP0    PHI
   :      :      :      :      :      :
. . .
----- POSITION
@ PHI_P    IPHIFIX
  90.      0
@ X0       Y0       Z0    IPOSFIX
  1.       0.       0.    0
  
```

# Example for Definition of 3D Data

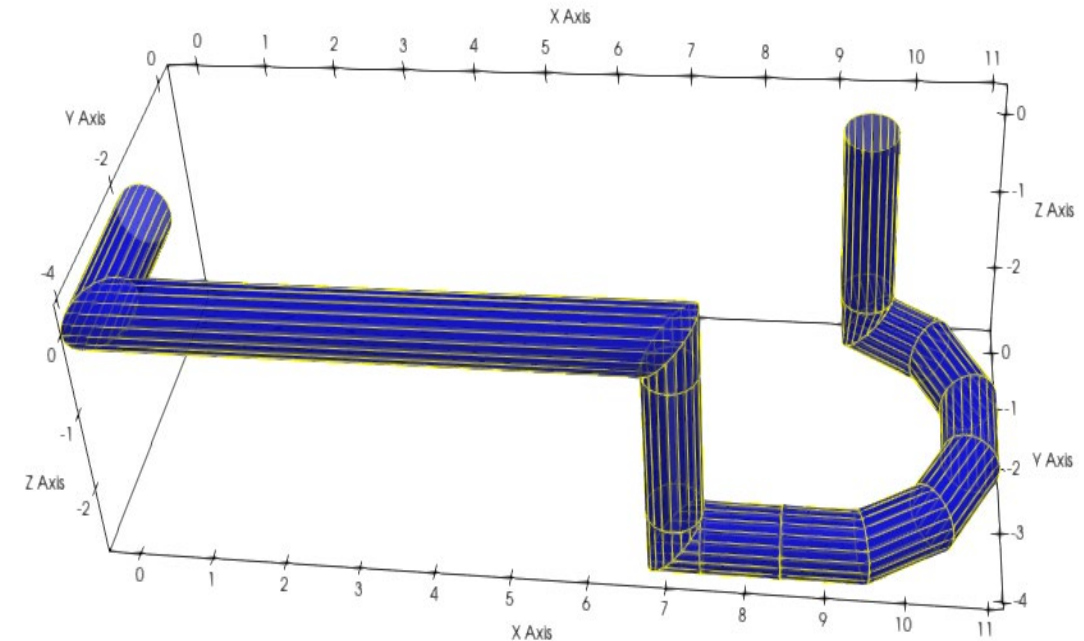
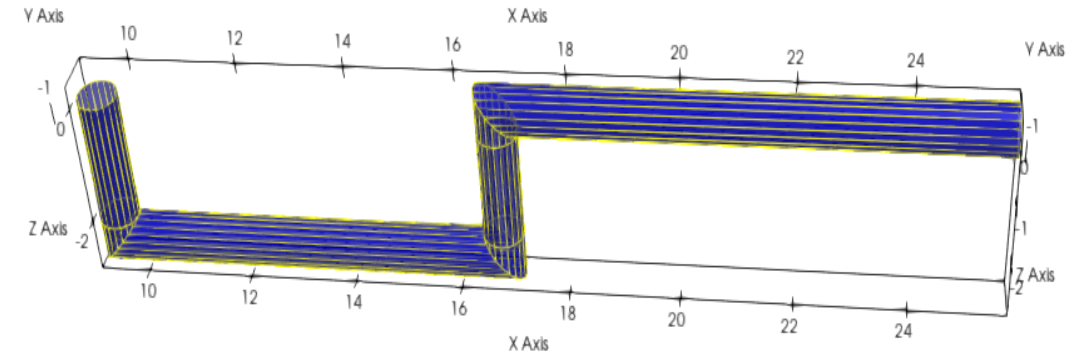
C---- PLUGIN  
vtk

C---- OBJECT  
.

----- GEOMETRY

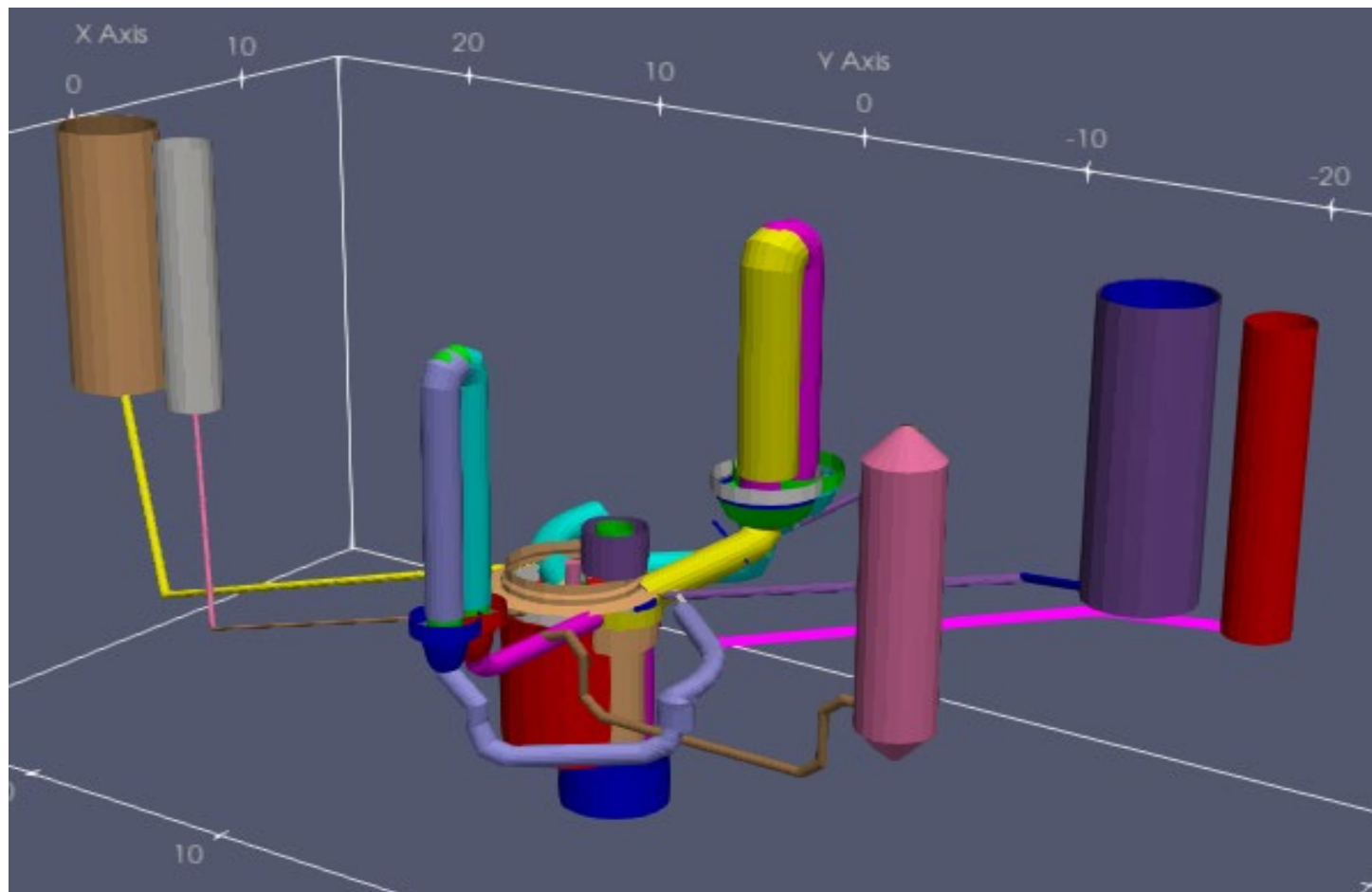
@	S0	Z0	D0	A0	V0	DEP0	PHI
	0.0	0.0	0.75	0.0	0.0	0.0	0.0
	2.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	3.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	4.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	5.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	6.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	7.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	8.5	-2.5	0.75	0.0	0.0	0.0	0.0
	9.5	-2.5	0.75	0.0	0.0	0.0	0.0
	9.84	-2.5	0.75	0.0	0.0	0.0	0.0
	12.34	0.0	0.75	0.0	0.0	0.0	0.0
	19.5	0.0	0.75	0.0	0.0	0.0	-90.0
	21.27	0.0	0.75	0.0	0.0	0.0	0.0

See sample1\_VTK.in



## VTK Plug-in

- Plug-in provided for generation of 3D object data in VTK format
- Enables visualization in ParaView
- All objects, TFOs and HCOs, represented by cylinders



***PWR Sample***

# New Input Option: Improved Control of Friction Loss Adaption

During SSC, input values for friction and form loss coefficients can be adapted by ATHLET

- control by input parameters IZETA0 and IPRI0
- to achieve a consistent state of the system
- Previously, a constant adaptation factor has been applied to all junctions within a priority chain

K----	PIPE		
@	ITYPO	FPARO	ICMPO
	20	1.	0
. . .			
-----	FRICTION		
. . .			
-----	SSCFRIC		
@	FADAPT		
	0.		
@	SJO	FADAPTJ	
	1.0	0.2	
	3.5	1.	

- Possibility to **restrict the adaptation to areas where information on pressure loss are incomplete** or unreliable
- **NEW PW SSCFRIC** under CW OBJECT
  - **FADAPT** switches on/off the adaptation for the complete TFO (PIPE or SJP)
  - $0. \leq \text{FADAPTJ} \leq 1.$  (de-)activates adaptation for individual junction near to position SJ0 (with given weight)
  - Overwrites PC-wide settings by IZETA0 and IPRI0



# New Input Data Options and Checks

- **Optional SW under TOPOLOGY** to switch on/off sets of priority chains
  - Improved configuration control, also via PARAMETERS
- **New GCSM controller types** allow specification of real-valued constants (CONST) and logical constants (LCONST)
- Input check for **unused parameters**
  - **New optional PW IDLE\_PARAM** under CW SERVICES
  - Quality assurance by detecting inadvertent input errors
- Additional input check for FUNGEN controller without X2NAME
  - IOPT must be -2 or 0
  - other options for IOPT cause a program stop now

```

C----- PARAMETERS
CONFIG_1 = S*----
CONFIG_2 = S-----
C----- TOPOLOGY
@      PRIORITY CHAINS
%CONFIG_1% COARSE
----- LOOP1

. . .
%CONFIG_2% FINE
----- LOOP1A

. . .
----- LOOP1B

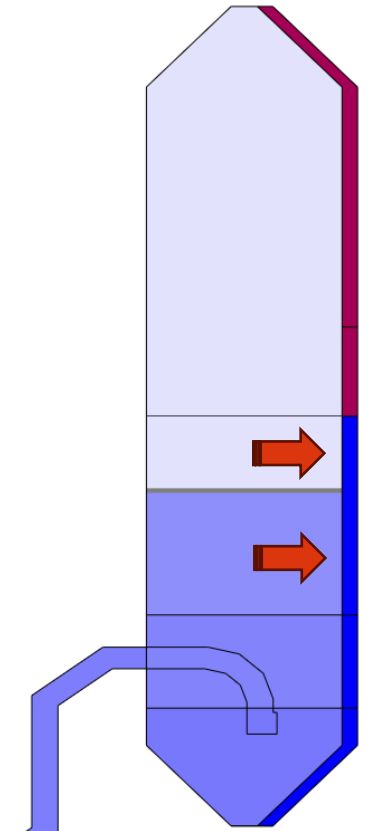
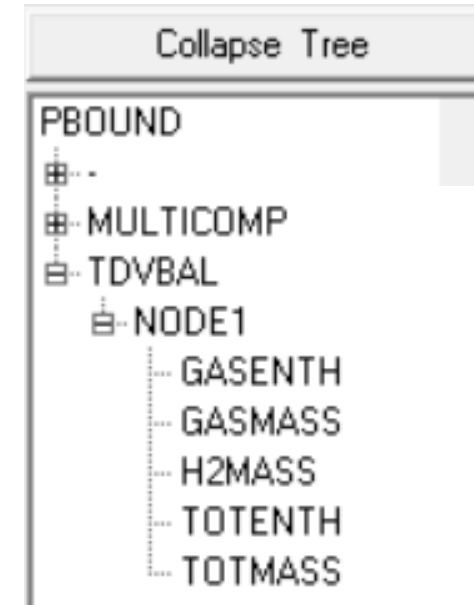
. . .

```

S-----	SPRAY	TEMPERATURE				
@	YNAME	CONTYPE	X1NAME	X2NAME	X3NAME	X4NAME
	STSPRAY	FUNGEN	TIME	-	TTSPRAY	-
@	IOPT	GAIN	A1	A2	A3	A4
	0	1.	0.	0.	0.	0.

# Additional Output Quantities

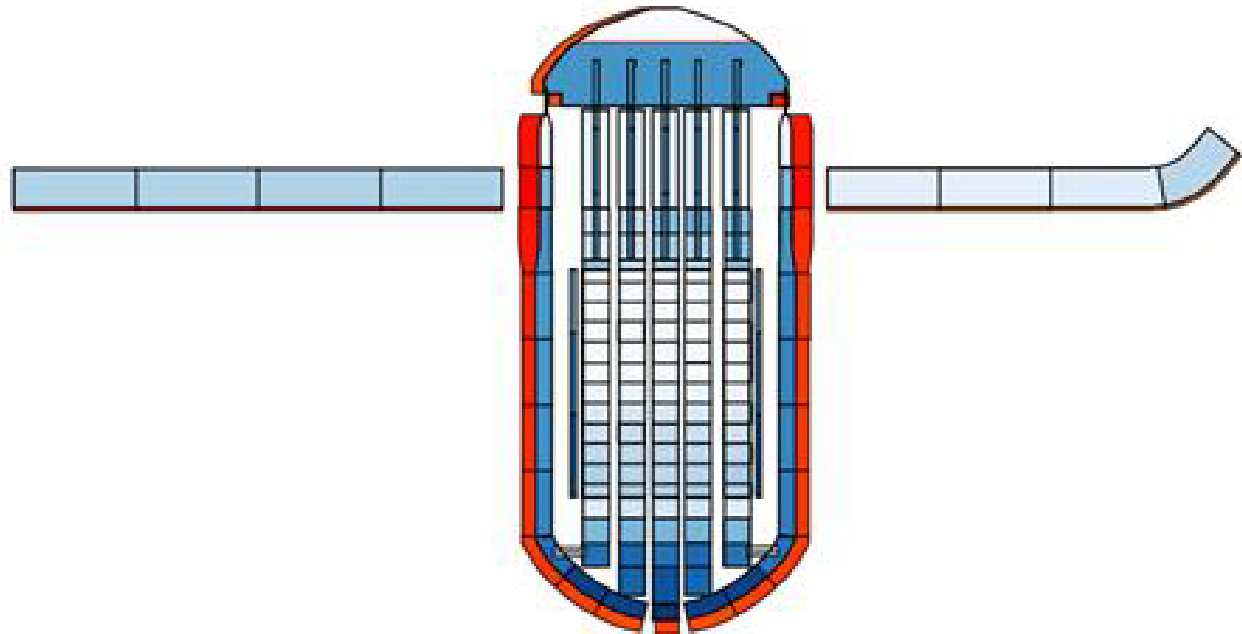
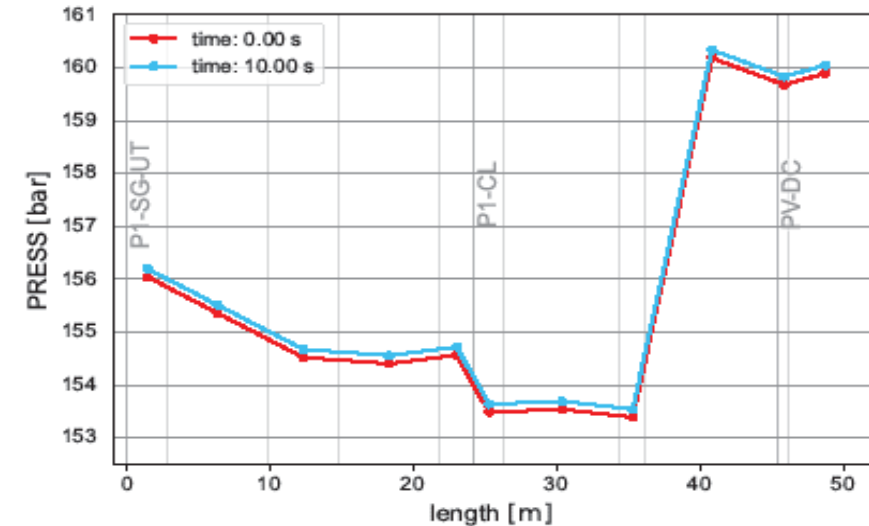
- **Integrated quantities for every TDV** (keyword TDVBAL)
  - Total (gas) mass and enthalpy flow towards/from the TDV
  - Mass flow per NC gas component
- Extended **balance quantities for TFD system** (TFDGENERAL)
  - Energy loss (ENLOSS): Integrated energy flow from TFD system into all connected HCOs except RODs and STEAMGENs
  - Total mass per NC gas component (e.g. NITMASS, OXYGENMASS,...)
- **HECU mixture level output under ML\_LEFT or ML\_RIGHT**
  - For mixture levels defined in TFOs on left/right side
  - Heat flows to sub-CVs QHLUP and QHLOW provided separately
  - Additional output for HTC, MODE, etc. for sub-CV above ML



ML_LEFT	I/J	IMLHL	INDHL	QHLUP	QHLOW	QLUP	QLLOW	HTCL	HTCVL	HTCCOL	HTCMIL	MODEL
	1	9	1	2.89E+06	7.18E+05	2.89E+06	7.18E+05	0.00E+00	0.00E+00	0.00E+00	4.39E+04	25

# Batchplot Plotting Tool

- Python based plotting tool for hdf5 and pd data
- **Platform independent**, for Linux and MS Windows
- Plotting **temporal, axial and radial (HCO) distributions**
- **New module to visualize 2D graphics from AIG**
  - Dynamic visualization via Jupyter notebook possible
  - For details and examples see Batchplot manual



# Summary

- **Numerous new and improved models in ATHLET 3.5**
    - Various new options for **detailed simulation of structures**, e.g. spacer grid model, 3D heat conduction, and new geometry type for horizontal plate
    - **New heat pipe module**, e.g. for investigation of **Micro Modular Reactors**
    - Improved modelling for **flow regimes and friction losses**
    - **User support and quality assurance** by extended input checks and output data
    - On-going integration of ATHLET and ATHLET-CD
- ➡ See **ATHLET Program Updates Manual** for complete listing

# Thank you for your attention!

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Reaktorsicherheit (GRS) gGmbH  
Schwertnergasse 1  
50667 Köln



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