

New Models and Features in ATHLET 3.5

Philipp Schöffel, GRS
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Content

- **New and Updated Models in ATHLET 3.5**
 - New models for **structures and internals**
 - Spacer grid modelling
 - Geometry, materials and heat conduction in HCOs
 - Extended **Flow Regime Maps and Friction Loss Models**
 - Component Model Updates: **Heat Pipe, Critical Discharge**
- **Input, Output and Postprocessing**
 - 3D TFO and HCO data
 - New Input Options and Output Data
- **Summary**

Modelling of Rod Bundles with Spacer Grids

Objective: Capture spacer grid effects on **TH behavior during core uncover**

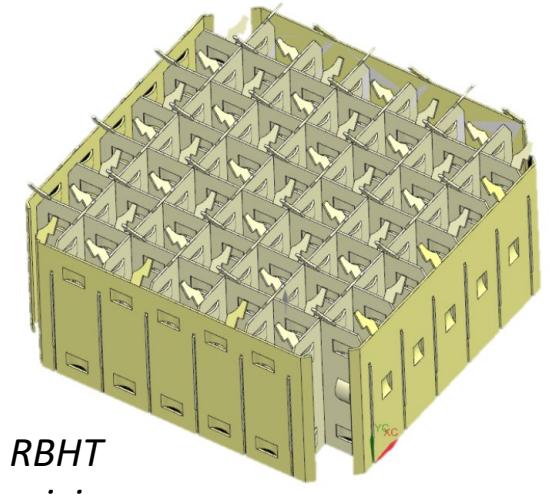
- **Convective heat transfer enhancement** downstream the spacer grid
- Increase of interfacial area and interfacial transfers due to **droplet breakup**

Previous ATHLET spacer grid model only considered impact on CHF

- Applicable with **Groeneveld LUT**

$$q_{\text{CHF,spacer}} = \left[1 + A \exp\left(\frac{-B L_S}{D_H}\right) \right] q_{\text{LUT}}$$

- Requires provision of input data under
 - PW SPACER (HECU) defining positions of spacer grids
 - PW FRICTION (TFD) with mandatory zeta value for each spacer grid junction

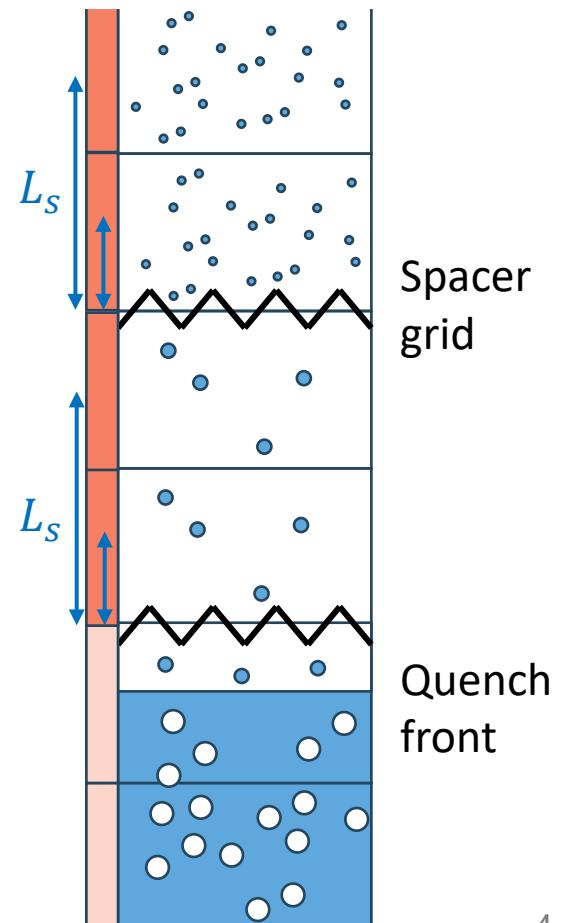


*RBHT
mixing vane
spacer grid*

C-----	HEATCOND		
K-----	HEATTRIN		
. . .			
-----	SPACER		
@ SHSPAC0 (1...N)			
0.102	0.690	1.212	. . .

Extended Spacer Grid Model

- Turbulence-induced **convective heat transfer enhancement** downstream the spacer grid
 - Model options depend on **blockage ratio ε or friction loss K_g**
 - Yao: $Nu_{\text{spacer}} = (1 + 5.55\varepsilon^2 e^{-0.13(L_s/d_h)}) \cdot Nu_0$
 - Holloway: $Nu_{\text{spacer}} = [1 + (0.8K_g - 0.4)e^{-0.25(L_s/d_h)}] \cdot Nu_0$
- Increase of interfacial area due to **droplet breakup**
 - **Reduced droplet Sauter mean diameter** downstream the grid, considered by evaporation model
$$\frac{d_{32}}{d_0} = 6.167 \cdot We^{-0.53}$$
 - Applied for dispersed flow regime
 - Considers quench front progression (if model is active)

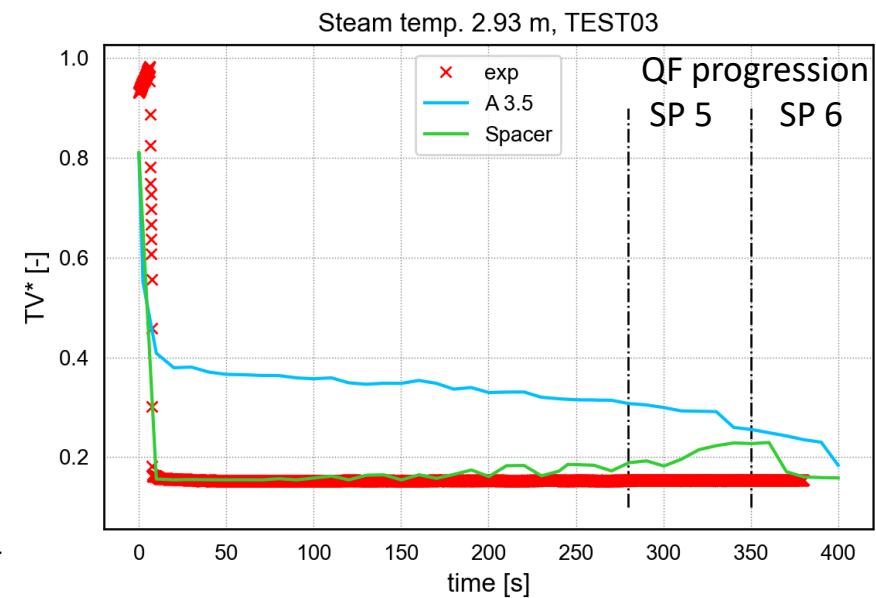
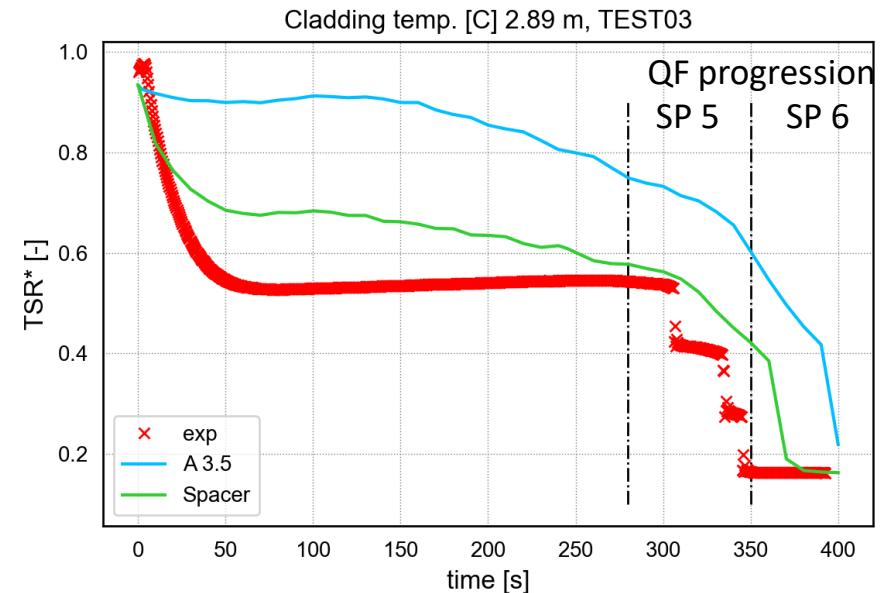
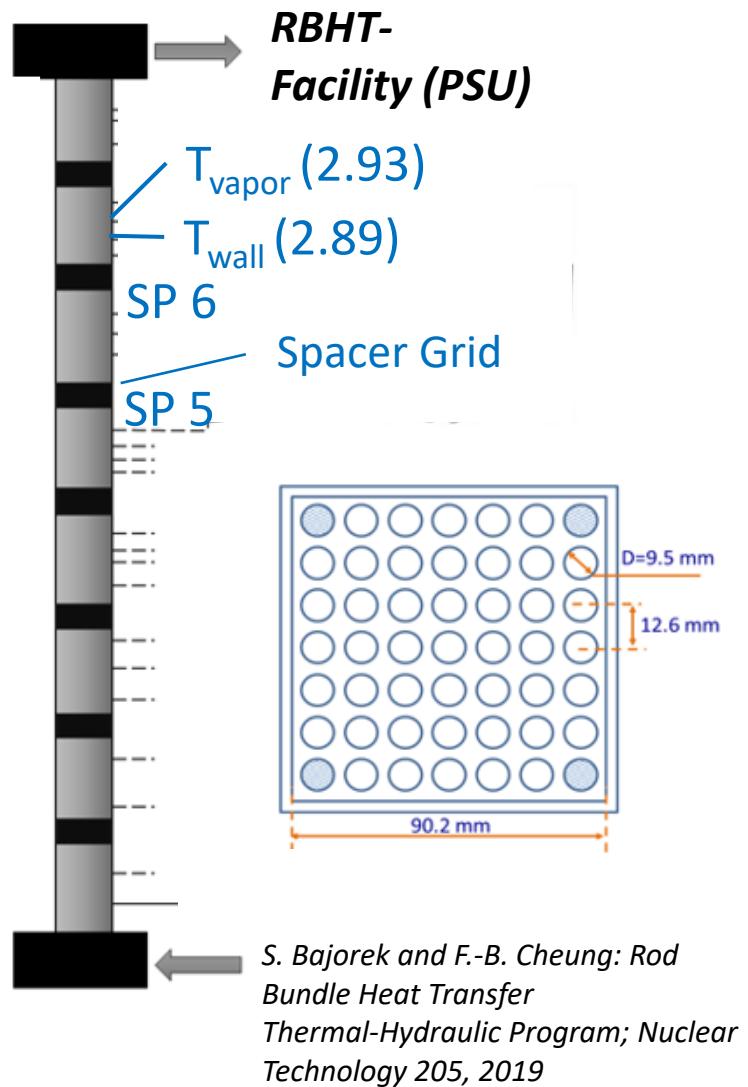


Validation against RBHT Experiment

OECD RBHT project

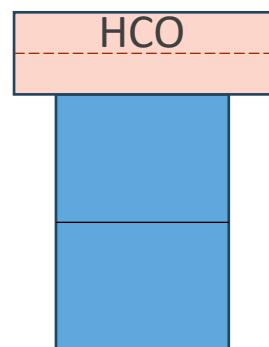
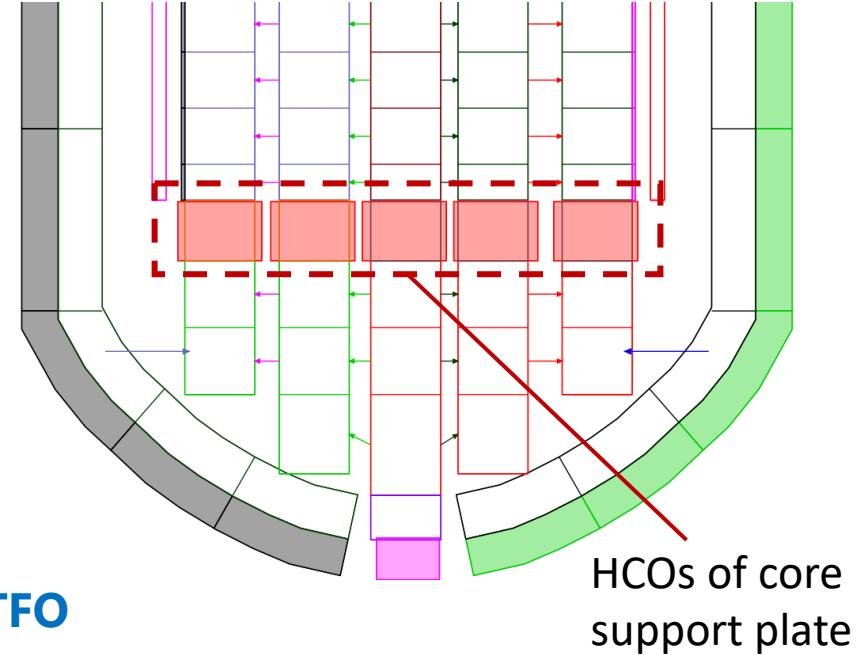
- Reflooding tests
- Pressure: 1 to 4 bar
- Subcooling: 3 to 80 K

Cladding precooling downstream of the spacer grid

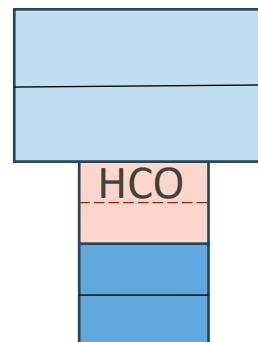


Simulation of Horizontal Structures

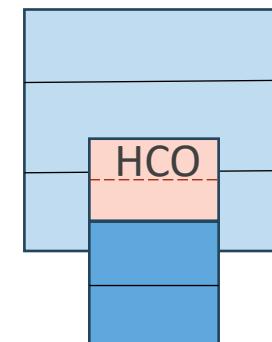
- Vessels or pools represented by vertically oriented TFOs
 - Up to now, coupling of an HCO only along axial direction of the corresponding TFO
 - **Limited accuracy** to model e.g. vessel lid, pool bottom, or a tie plate
 - **Need to couple an HCO orthogonally to a vertical TFO**
- **New HCO type “horizontal plate”** introduced
 - enables to couple a strictly horizontal HCO orthogonally to a (strictly vertical) CV
 - always consists of a single HCV



one-sided coupling



two-sided coupling



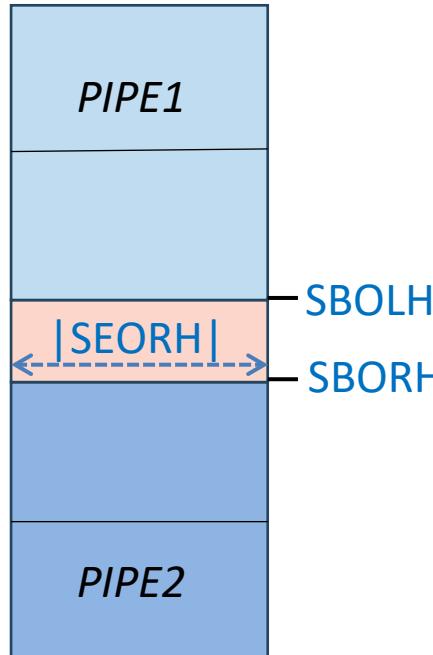
coupling inside CV

Application of Horizontal Plate

```

K---- HORPLATE
@ AOLH  SBOLH  SEOLH  AORH  SBORH  SEORH
  PIPE1    0.  -0.2  PIPE2    5.  -0.2
@ . . .  IGE00  ...
  . . .    0  ...
----- GEOMETRY
...
@ SG0  Z0  DI0  DS10  GAP10  ...
  0.  1.3  0.15  0.05  0.      ...
  0.2  1.3  0.15  0.05  0.      ...

```



- **By convention, the left side is the upper side**, the right side the lower side
- Coupling location inside the TFO is determined by SBOLH resp. SBORH
- A negative input value for SEOLH or SEORH indicates horizontal coupling. Its absolute value must be equal the length of the plate.

- Horizontal plate during application:
 - **Churchill correlation** for natural convection heat transfer at top and bottom side:
 - No specific correlations in other heat transfer regimes

$$Nu = c \cdot \left[Ra \cdot \left[1 + \left(\frac{d}{Pr} \right)^a \right]^{-1/a} \right]^b$$

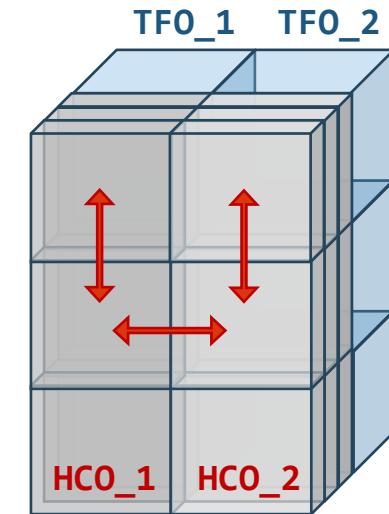
New Options for Structure Materials

- HCOs may optionally consist of **more than three material zones**
 - **Input parameter NADDMZ:** number of additional zones
 - Extension of further PWs where relevant, e.g. GEOMETRY, HTCDEF, MATPROP
- Additional built-in materials available: **BORCARBIDE, INCONEL600, ALUMINA** (Al_2O_3)

```
K---- H_BOILER  @ split into 6 material zones
@ AOLH          SBOLH  SEOLH  AORH          SBORH  SEORH
          ADIABAT    0.     0.     BOILER        0.02   0.07
@ NIHCO N10 N20 N30 IGE00 ICOMPO ACOMP0  ICHF0 NADDMZ
      1     10    2     2     5     0     DUMMY     2     3
@ N40  N50  N60
      2     2     2
@----- GEOMETRY
. . .
----- HTCDEF
```

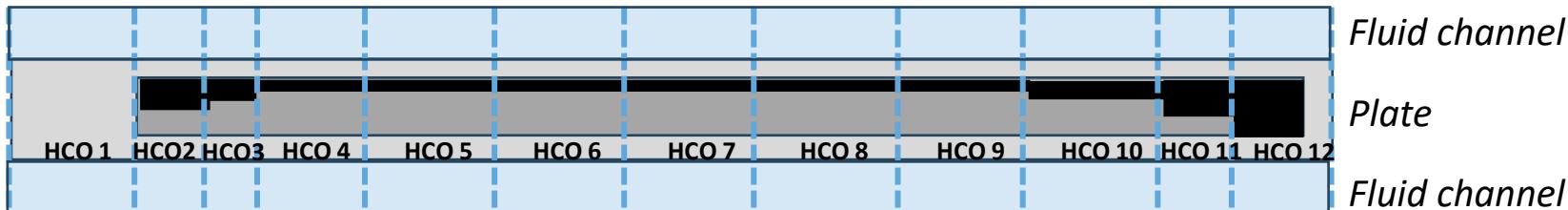
Simulation of 3D Heat Conduction in Structures

- **Motivation:** Detailed simulation of complex structural components
 - Usage of a 3D TFD network requires refining the HCO network
 - So far, HECU solved for a 1D or a pseudo-2D heat conduction equation
- **New CW HCOCONNECT** enables **3D heat conduction** by coupling of HCOs
 - Prerequisite: equal axial nodalization and equal number of layers
 - Alternative sparse matrix solver from PETSc package
- **Application:** plate-type fuel elements in research reactor *



```

C----- HCOCONNECT
@  IHCSYS
  4
K----- Group1
  .
  .
  .
@  AHCOLIST(1,...,n)
  HCO_1  HCO_2  ...
  
```

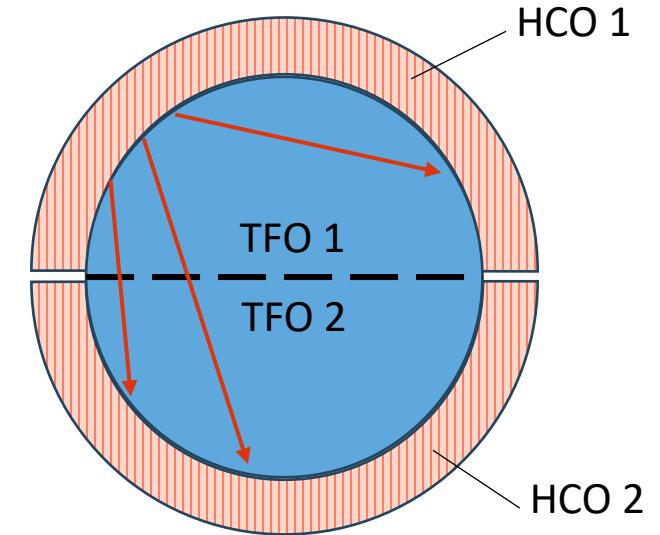


* See presentation by F. Weyermann

Extended Thermal Radiation Model

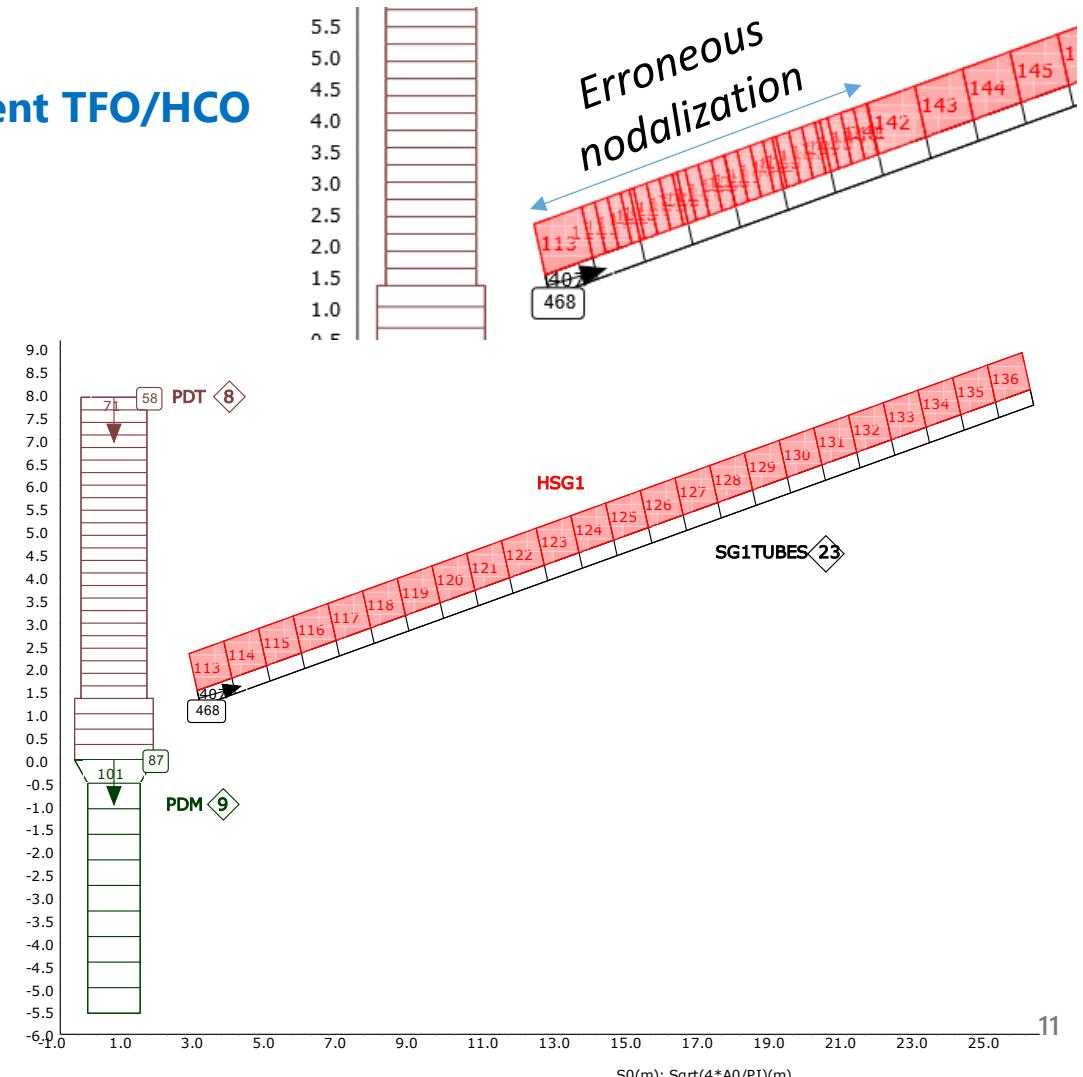
Thermal radiation between HCOs connected to *different* TFOs

- Definition of radiation group under **new KW FLEXRAD**
- All grouped HCOs must have the same length
- Optional shape factor s for energy flux: $E = s \cdot \epsilon \cdot \sigma \cdot T^4$
- **Additional input check** to ensure reciprocity: $A_1 \cdot \varphi_{1 \rightarrow 2} = A_2 \cdot \varphi_{2 \rightarrow 1}$



Improvements of HECU Module for Helically Coiled HTEX

- Inside helical heat exchanger tube, **HTC calculation under film boiling conditions** uses Mc Eligot correlation (avoids program error)
- Improved automatic **HCO nodalization for non-congruent TFO/HCO**
 - Helical coil represented by inclined pipe
 - Erroneous HCO nodalization results caused program stop
 - Depending on orientation of inner and outer side TFOs
 - Work around: introduce numerous HCOs each consisting of one HCV
 - Improved program implementation provides HCO **nodalization that matches both adjacent TFOs**
 - Increased user friendliness**



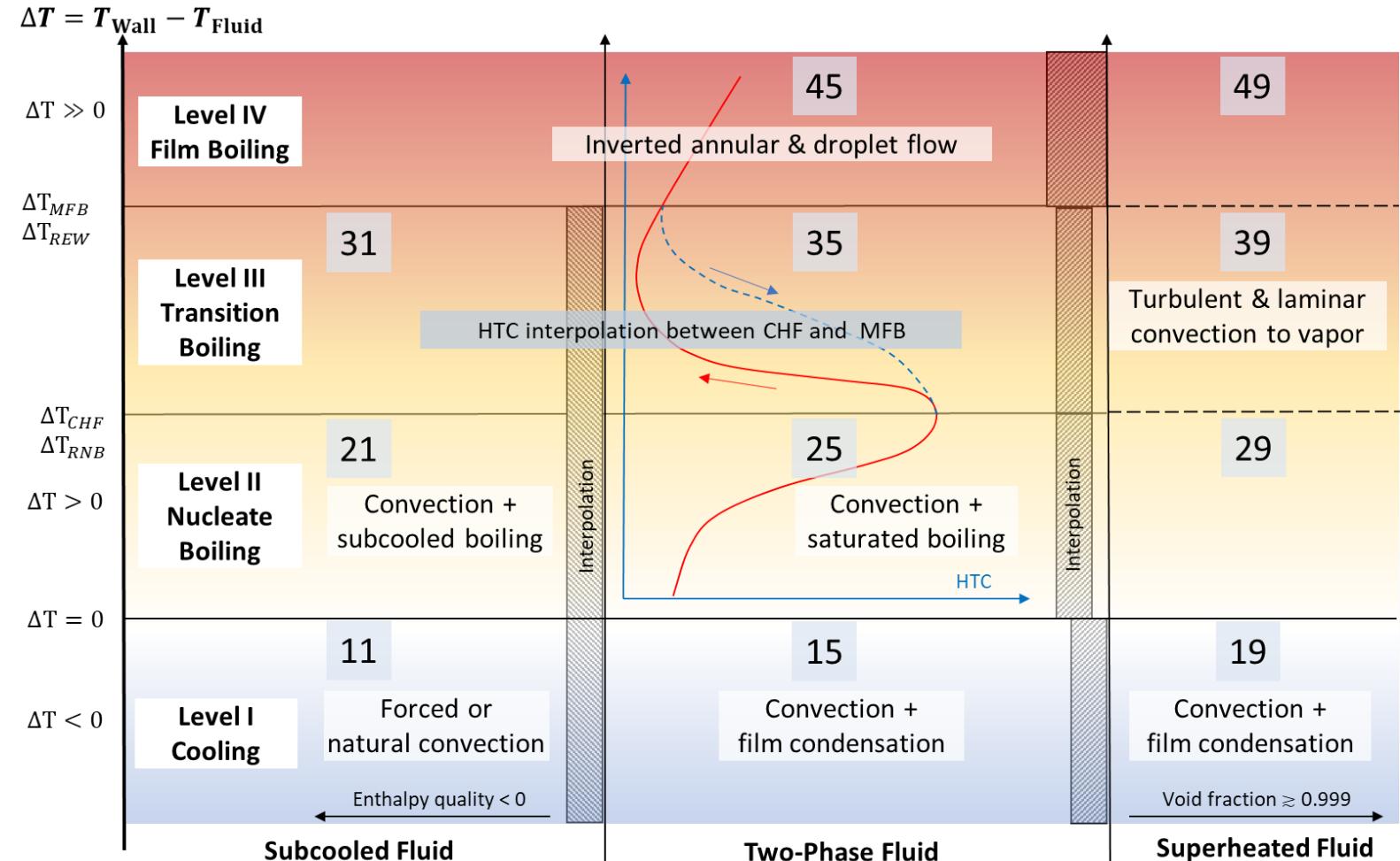
Extended Plug-ins for User-provided HTC and CHF Correlations

MHTCEXT plug-in

- Comprises set of interfaces for various heat transfer regimes and working fluids
- **New interface** for convective heat transfer to vapor in **DFFB regime (mode 49)**

Extended CHF plug-in

- Interface provides **access to TH quantities at core channel entry**
- **OMP-safe access to ATHLET global variables** via plug-in function *execute_c*

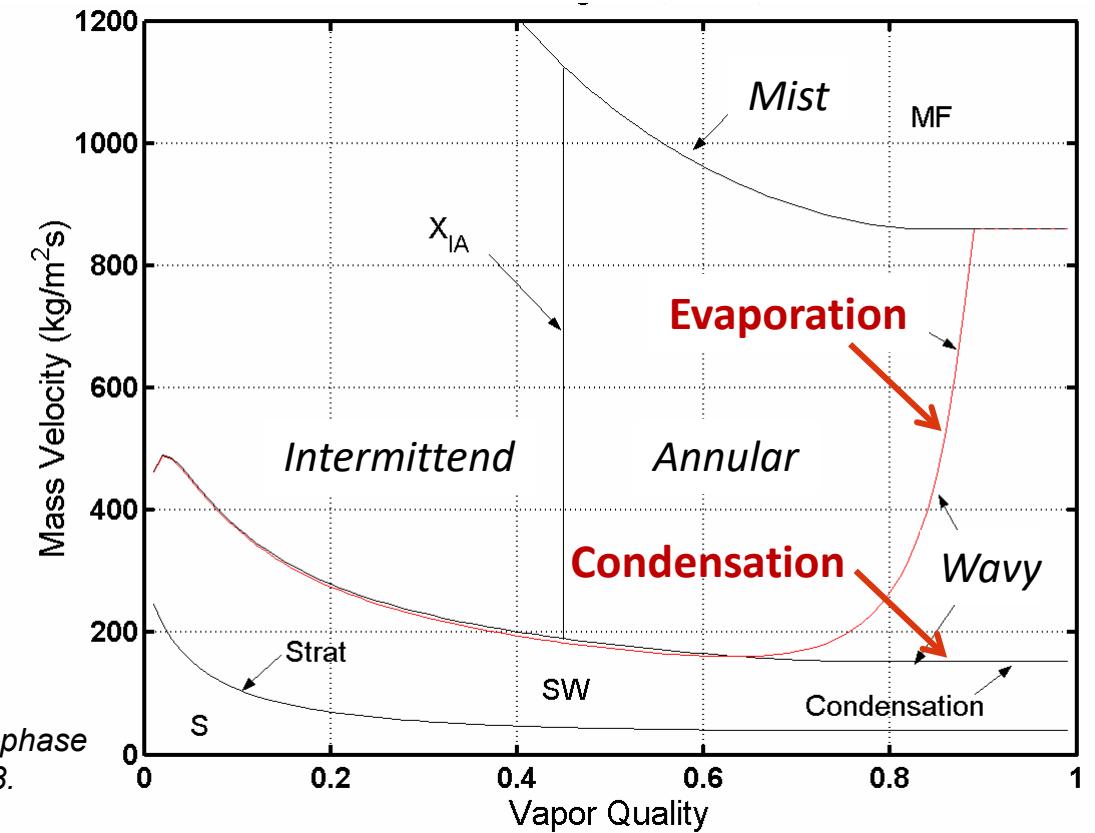


Unified and Extended Flow Regime Maps

- **Motivation:** Use of dedicated flow regime maps for both boiling as well as condensing flows
 - Centralized flow regime calculation (based on Taitel-Dukler) with **unified flow pattern map**
 - Unified calculation of the entrained liquid fraction
 - Output of current flow regime
- For **flows with wall condensation (passive systems)**
 - **Adjusted flow regime map** focusing on **horizontal annular flow**
- Steady transition between flow regime maps for

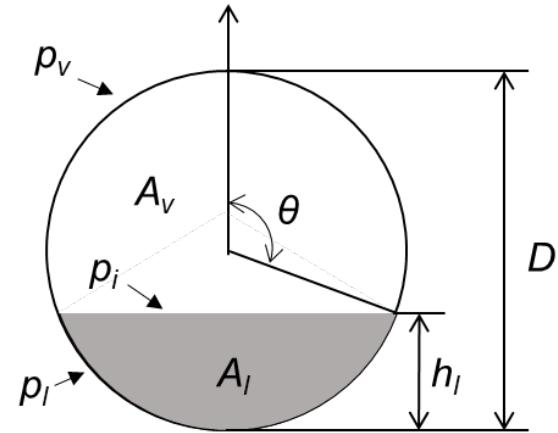
$$-1 \text{ }^{\circ}\text{C} \leq T_{\text{wall}} - T_{\text{sat}} \leq 0 \text{ }^{\circ}\text{C}$$
- Optional model, to be activated under
CW MISCELLAN

* Hajal, J. E., Thome, J. R., Cavallini, A.: Condensation in horizontal tubes, part 1: two-phase flow pattern map. International Journal of Heat and Mass Transfer, Bd. 46, Nr. 18, 2003.



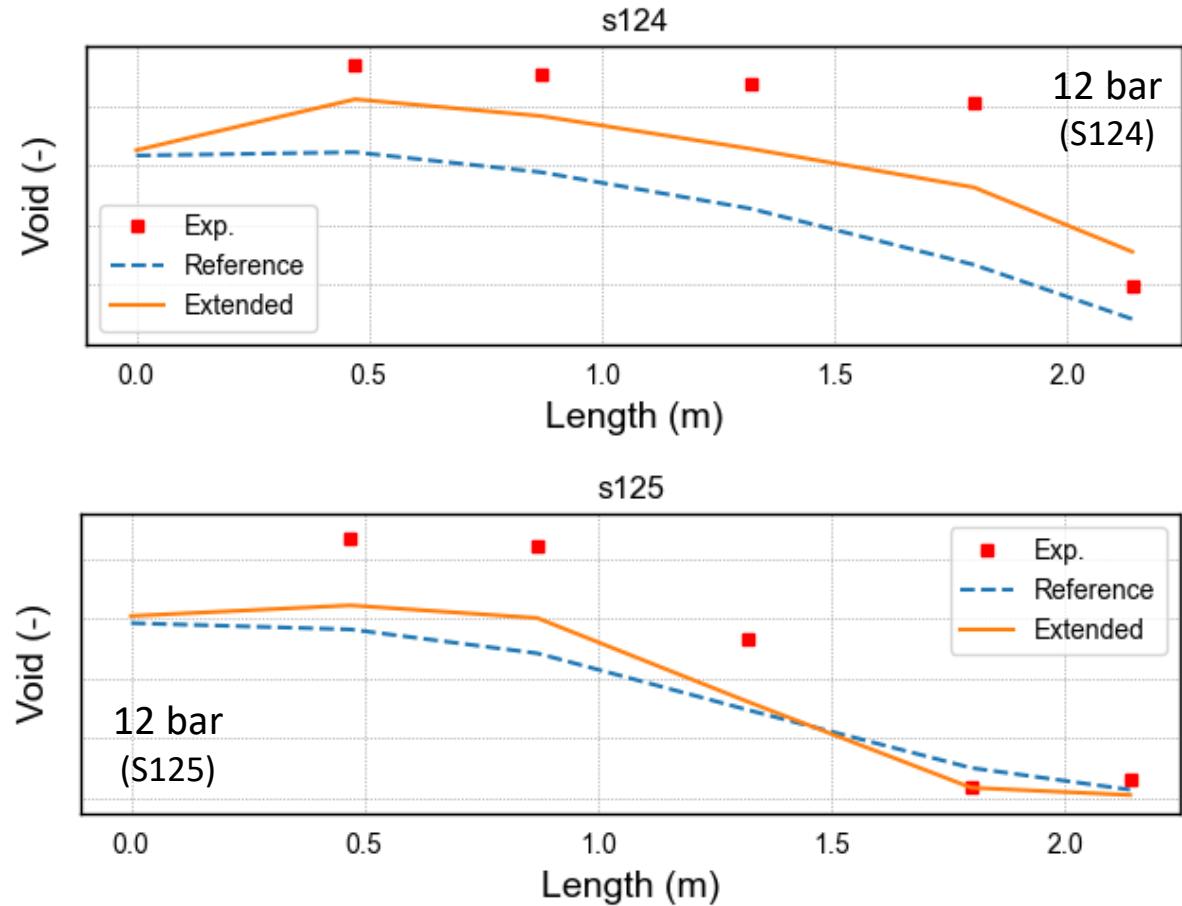
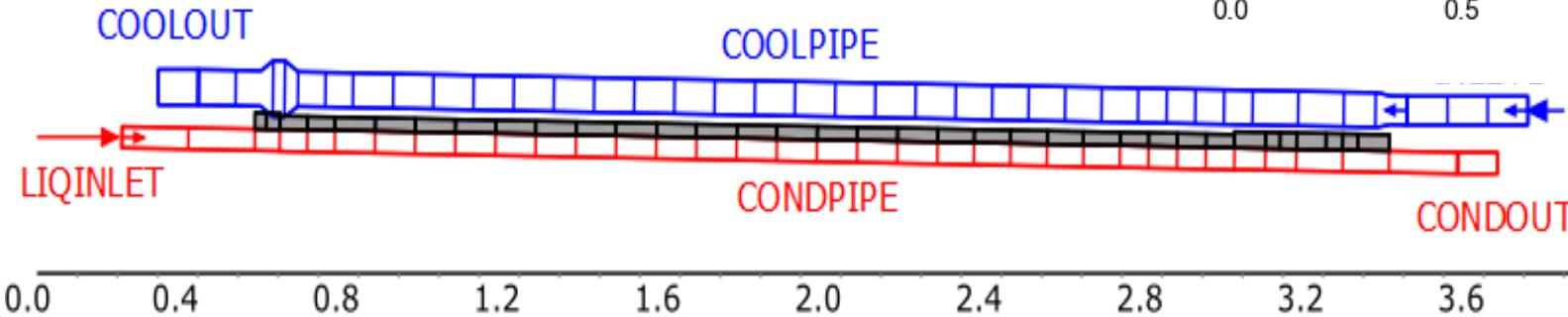
Closure Laws for Flow Regimes with Wall Condensation

- Dedicated closure laws for **annular flow and stratified/stratified wavy flow**
- **Interfacial friction**
 - $C_{i,str} = \frac{1}{2} \rho_v \lambda_v \frac{4 \sin \theta}{D_h \pi}$ (Taitel-Dukler)
 - $C_{i,wavy} = \frac{1}{2} \rho_v \lambda_v \left(1 + 15 \left(\frac{h_l}{D_h} \right)^{0.5} \left(\frac{j_v}{j_{v,crit}} - 1 \right) \right) \frac{4 \sin \theta}{D_h \pi}$ (Andritsos-Hanratty)
 - $C_{i,ann} = \frac{1}{2} \rho_v 0.005 [1 + 75(1 - \alpha)] \frac{4}{D_h} \sqrt{\alpha}$ (Wallis)
- **Wall friction** distribution to phases according to dry / wetted perimeter
 - Annular flow: wall friction completely assigned to liquid phase



Validation of Flow Regime Map Module for Horizontal Pipe

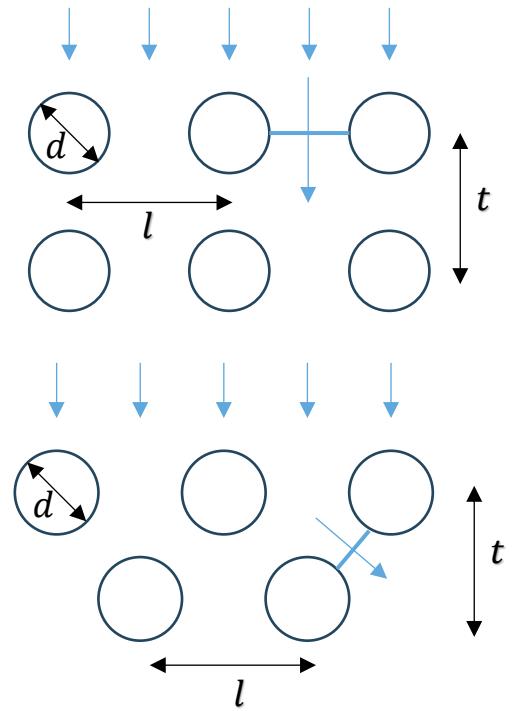
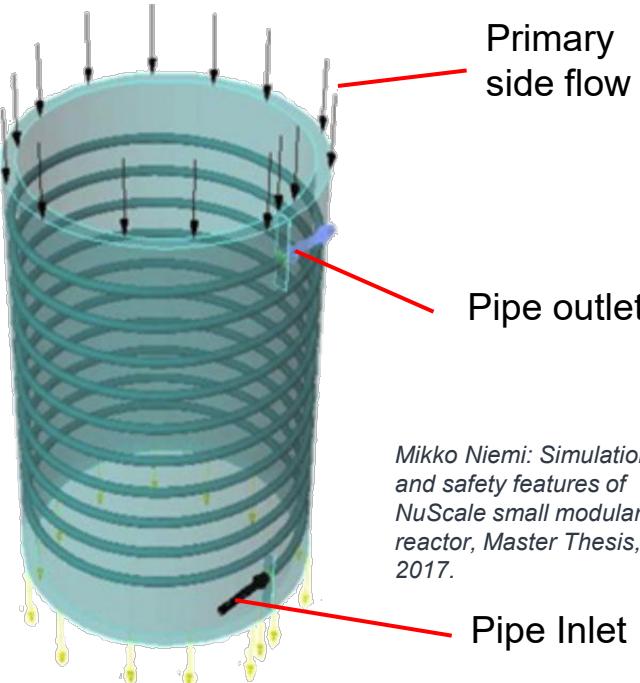
- **COSMEA experiment** with coaxial double pipe
- Slightly inclined pipe ($L = 2.82$ m, $D = 43$ mm)
- Condensation of steam in inner pipe
- On-going work related to
 - **Wall heat flow distribution** to phases
 - **Harmonization of wall condensation and bulk condensation models**



Friction Loss for Special Components

Cross flow in bundle (in-line or staggered arrangement)

- friction loss ζ dependent on Reynolds number $\zeta = \zeta_{\text{lam}} + \zeta_{\text{turb}} \cdot F(Re)$
- Dedicated correlation to be activated via CW FORMLOSS
- Automatically employed for helical heat exchanger (PW HTEXDEF)



For helical heat exchanger (inner side)

- Modified friction factor *: $\lambda_{\text{helix}} = \lambda_{\text{turb}} \left(Re \left(\frac{d_h}{d_{\text{coil}}} \right)^2 \right)^{1/20}$
- 2-phase flow with modified Martinelli-Nelson multiplier Φ_{tt}
- Development by RUB/J. Krieger **

* Nariai et al.: Friction pressure drop and heat transfer coefficient of two-phase flow in helically coiled tube once-through steam generator, J. Nucl. Sic. Technol. 19, 1982

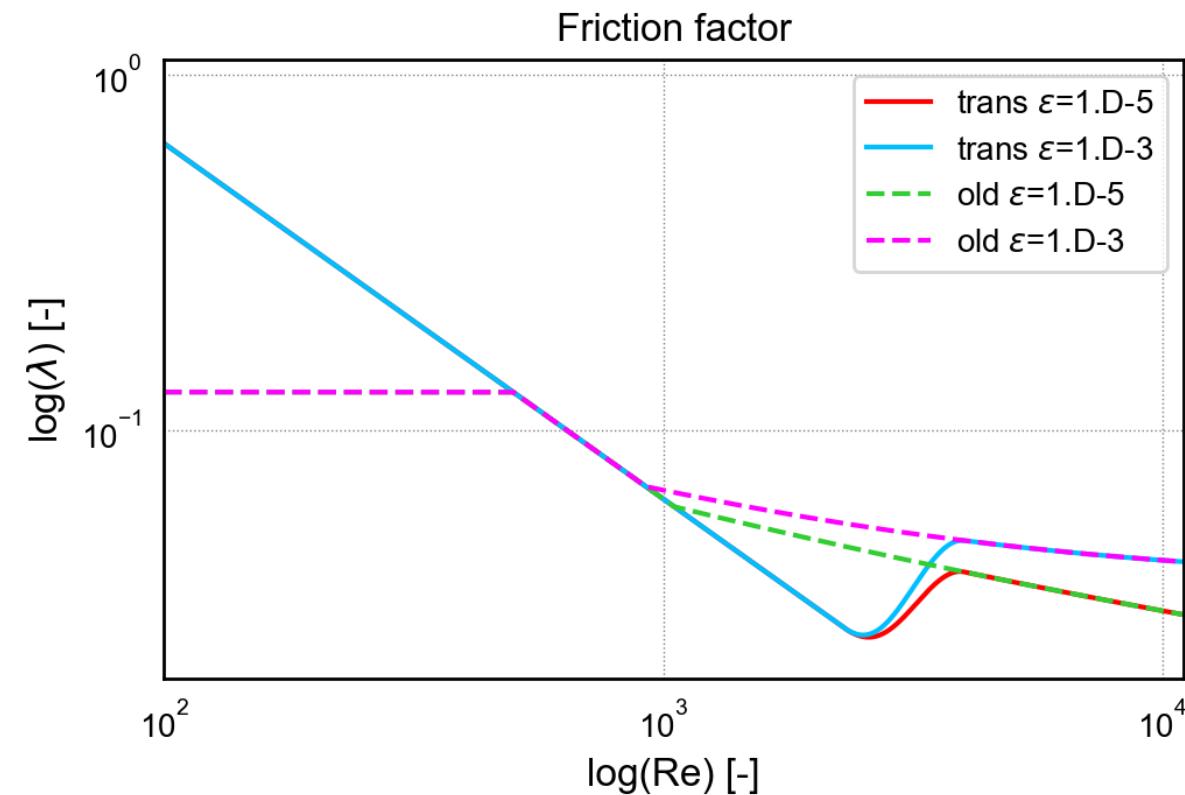
** Krieger et al.: Simulation of the experiment OSU-002 regarding the behavior of a helically coiled steam generator using AC²-ATHLET, ICONE30, 2023

Wall Friction in Laminar-turbulent Transition

Motivation: improved calculation of wall friction at **low Re-numbers** (IKE, M. Abd El Malek)

- **Start-up behavior of passive systems**
- So far, Darcy-Weisbach friction factor as maximum of Hagen-Poiseuille and Colebrook: $\lambda = \max(\lambda_{\text{lam}}, \lambda_{\text{turb}})$
- **Improved model with cosine-shape transition** between λ_{lam} and λ_{turb} for $2300 \leq Re \leq 4000$
 - For laminar flow: limitation of λ to $Re_L \geq 5$
 - Default model for pipe and annulus geometry
 - Input parameter **ITRNS** to select friction model
 - Adjustable Reynolds **interpolation range**

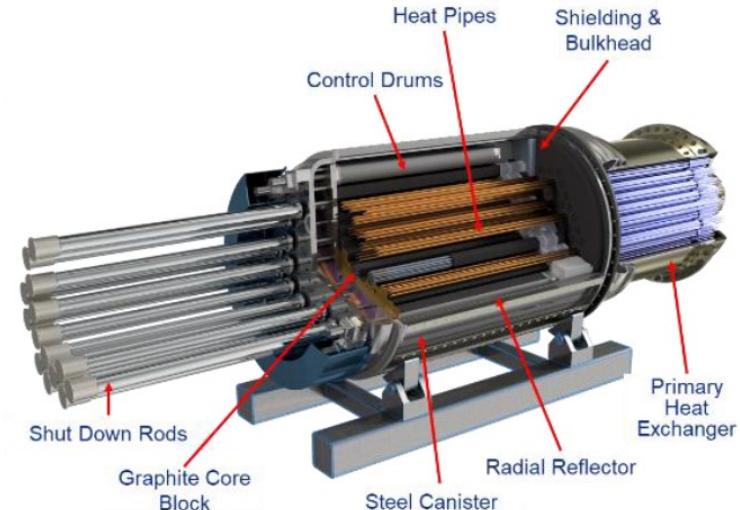
```
----- FRICTION
@      ITPMO    ALAMO    ROUO
      2          1.0      1.D-5
@      ITRNS    TRNS1    TRNS2
@      1          2000.   3000.
```



New Feature: High-Temperature Heat Pipe Module

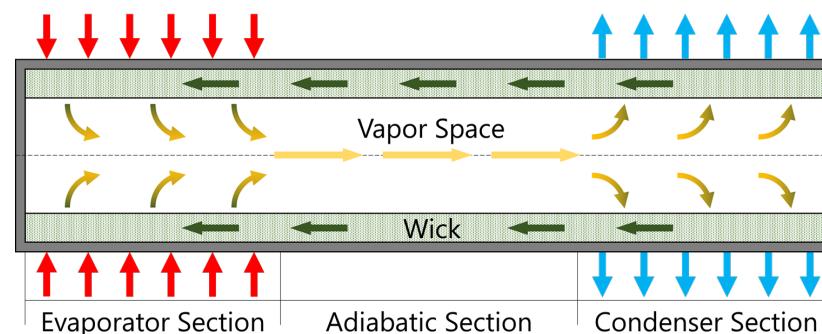
- **Liquid metal heat pipe-cooled MMR** (eVinci, SPR, ...)
- Development of ATHLET for MMR safety analysis
- ATHLET Heat Pipe Module comes with **specific models ***
 - **Wick structure, capillary pumping, phase change, friction loss**
 - Covers **different wick types** and materials
 - Working fluids: Sodium, Potassium
 - Works with NC gases
 - For horizontal and vertical heat pipes

* Details in presentation by D. Eckert



eVinci reactor system overview

Hong Xu, Yizhou Yan, Oriol Noguera Oliva,
 "CFD Thermal Analysis for Primary Heat
 Exchanger of eVinci™ Nuclear Test Reactor",
 21th International Topical Meeting on Nuclear
 Reactor Thermal Hydraulics, Busan, South
 Korea, August 31th - September 5th 2025



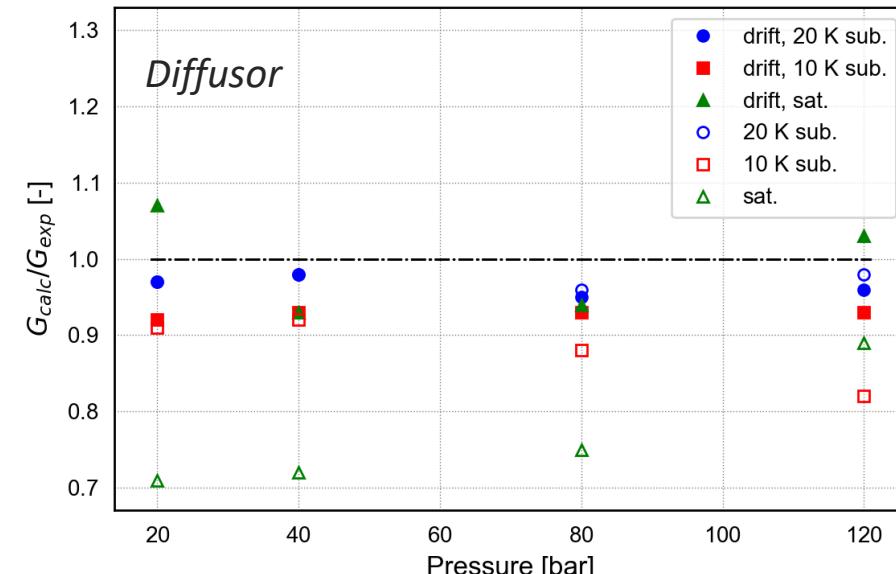
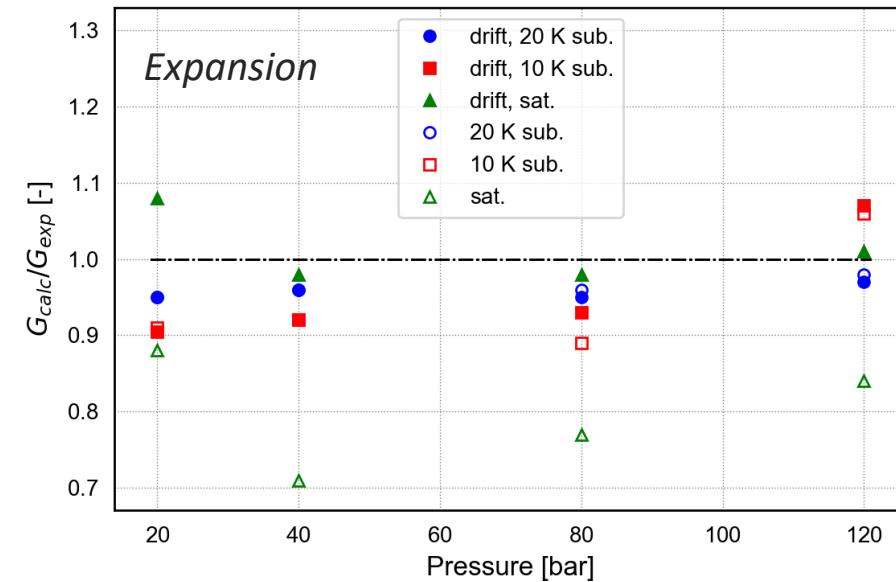
New Option for Critical Discharge Rate Calculation

Critical discharge model CDR1D extended by optional consideration of phase drift

- 4-eq. system with phase slip

$$S = 1 + \frac{3}{2} \sqrt{3\alpha} (1 - \alpha) \left(\left(\frac{\rho_l}{\rho_v} \right)^{1/3} - 1 \right)$$

- Application of ATHLET standard evaporation model:
 - Input parameter **TURB defines bubble number density**
- Activated under CW DISCHARGE: IAUR=5
- Validation against Super Moby Dick experiment
 - 20 mm nozzle
 - Two different geometries investigated: Sudden expansion or diffusor
- Further model validation required



Integration of ATHLET-CD

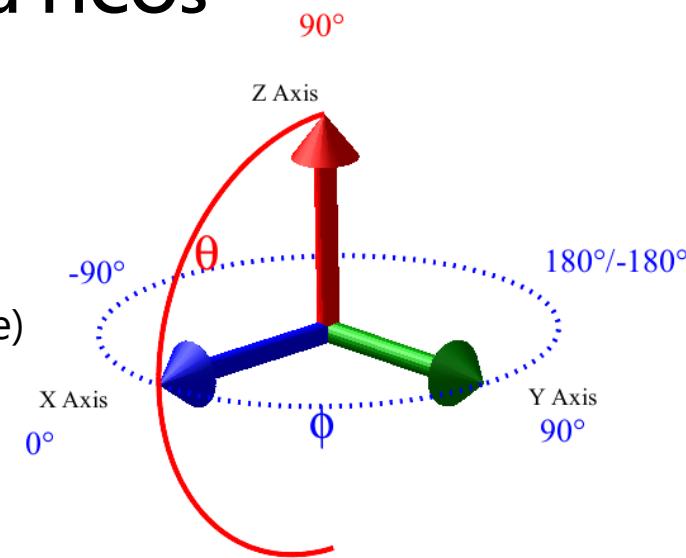
- **Ongoing ATHLET-CD integration into ATHLET** makes several modules available *

 - VENTINA for initial inventory calculation and decay of isotopes
 - FPREL and SAFT for release, transport and deposition of radionuclides in LWR
 - THEMEC for fuel rod behavior, ballooning, and feedback on thermal-hydraulics (blockage)
 - Enables accident simulation without core degradation/until melting

* Details in presentation by L. Lovasz

New Input and Output Options: 3D Data for TFOs and HCOs

- **Motivation:** Extend ATHLET by 3D information
 - Compact 3D graphical system representation
 - Future usage of 3D data by physical models (e.g. thermal radiation in 3D core)
- **Basic geometry information** derived from CW TOPOLOGY
- Additional 3D data from **optional extension of PW GEOMETRY**
 - **rotation angle Φ in XY plane**
- Optional input under **new PW POSITION**
 - Rotation angle and (x,y,z) coordinate at TFO origin
 - Parameters to define if data are absolute or relative to preceding TFO
 - Positioning of first TFO of each TFD system
 - Easy copying of TFOs with different spatial orientation
 - Note: changes in height position influence TH simulation



C----- OBJECT							
. . .							
----- GEOMETRY							
@	SG0	Z0	D0	A0	V0	DEPO	PHI
:	:	:	:	:	:	:	:
. . .							
----- POSITION							
@	PHI_P	IPHIFIX					
	90.	0					
@	X0	Y0	Z0	IPOSFIX			
	1.	0.	0.	0			

Example for Definition of 3D Data

C---- PLUGIN

vtk

...

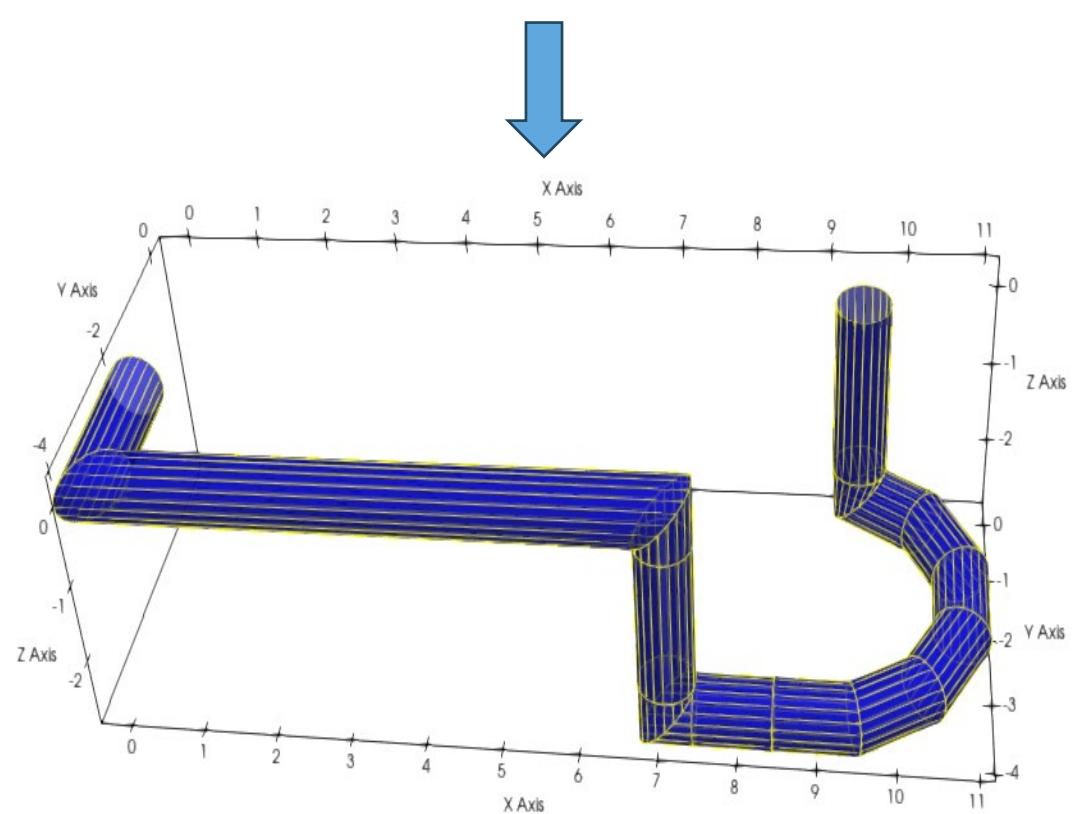
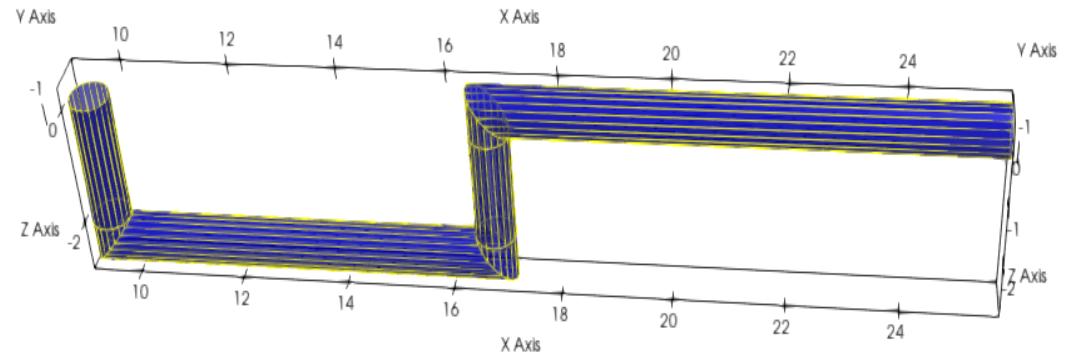
C---- OBJECT

...

----- GEOMETRY

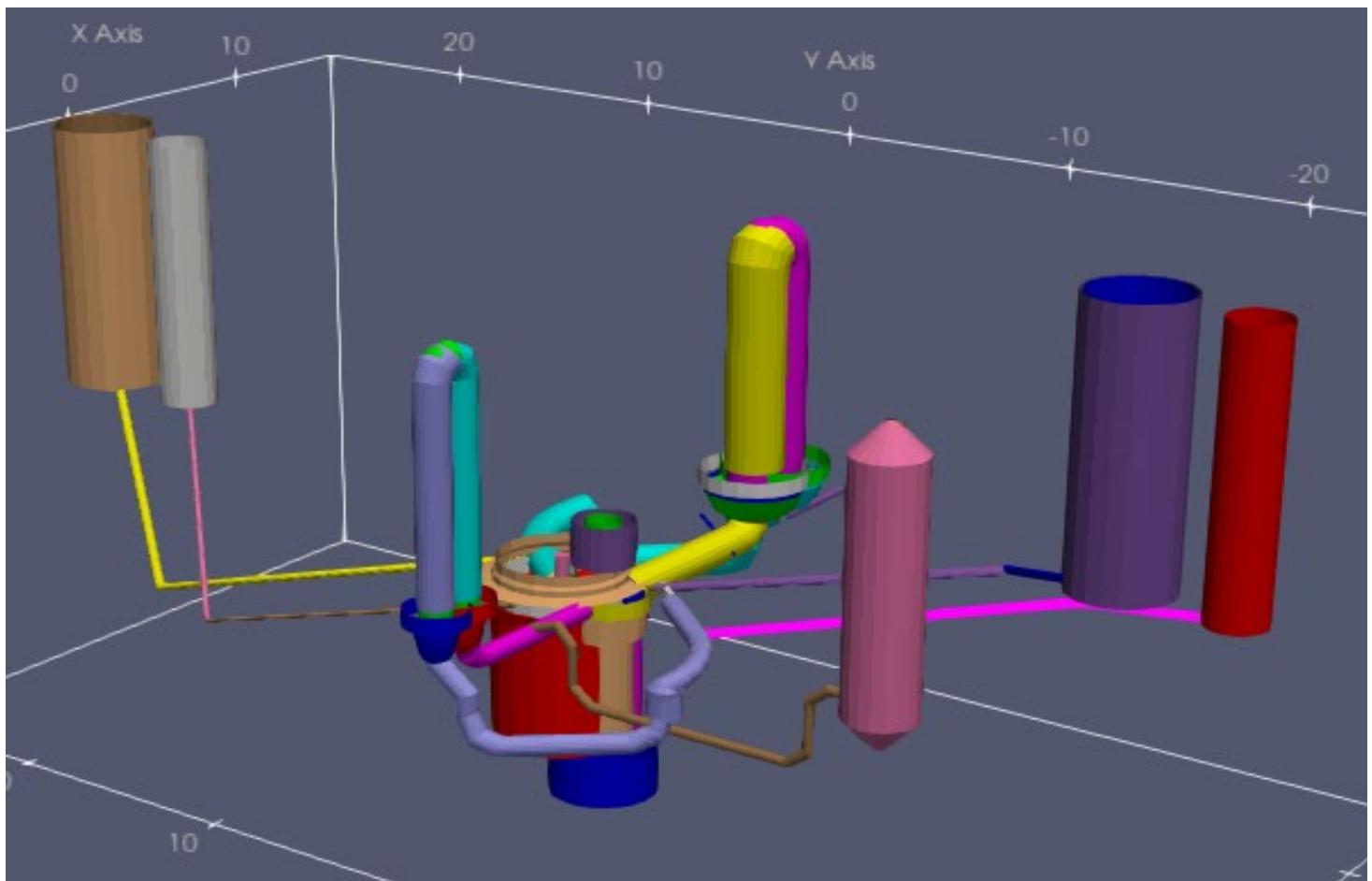
@	S0	Z0	D0	A0	V0	DEP0	PHI
	0.0	0.0	0.75	0.0	0.0	0.0	0.0
	2.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	3.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	4.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	5.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	6.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	7.5	-2.5	0.75	0.0	0.0	0.0	-30.0
	8.5	-2.5	0.75	0.0	0.0	0.0	0.0
	9.5	-2.5	0.75	0.0	0.0	0.0	0.0
	9.84	-2.5	0.75	0.0	0.0	0.0	0.0
	12.34	0.0	0.75	0.0	0.0	0.0	0.0
	19.5	0.0	0.75	0.0	0.0	0.0	-90.0
	21.27	0.0	0.75	0.0	0.0	0.0	0.0

See sample1_VTK.in



VTK Plug-in

- Plug-in provided for generation of 3D object data in VTK format
- Enables visualization in ParaView
- All objects, TFOs and HCOs, represented by cylinders



New Input Option: Improved Control of Friction Loss Adaption

During SSC, input values for friction and form loss coefficients can be adapted by ATHLET

- control by input parameters **IZETA0** and **IPRI0**
- to achieve a consistent state of the system
- Previously, a constant adaptation factor has been applied to all junctions within a priority chain

```
K---- PIPE
@ ITYPO      FPAR0      ICMPO
  20          1.          0
.
.
.
----- FRICTION
.
.
.
----- SSCFRIC
@ FADAPT
  0.
@ SJ0      FADAPTJ
  1.0        0.2
  3.5        1.
```

- Possibility to **restrict the adaptation to areas where information on pressure loss are incomplete** or unreliable
- **NEW PW SSCFRIC** under CW OBJECT
 - **FADAPT** switches on/off the adaptation for the complete TFO (PIPE or SJP)
 - $0. \leq FADAPTJ \leq 1.$ (de-)activates adaptation for individual junction near to position SJ0 (with given weight)
 - Overwrites PC-wide settings by **IZETA0** and **IPRI0**

New Input Data Options and Checks

- **Optional SW under TOPOLOGY** to switch on/off sets of priority chains
 - Improved configuration control, also via PARAMETERS
- **New GCSM controller types** allow specification of real-valued constants (CONST) and logical constants (LCONST)
- Input check for **unused parameters**
 - **New optional PW IDLE_PARAM** under CW SERVICES
 - Quality assurance by detecting inadvertent input errors
- Additional input check for FUNGEN controller without X2NAME
 - IOPT must be -2 or 0
 - other options for IOPT cause a program stop now

```

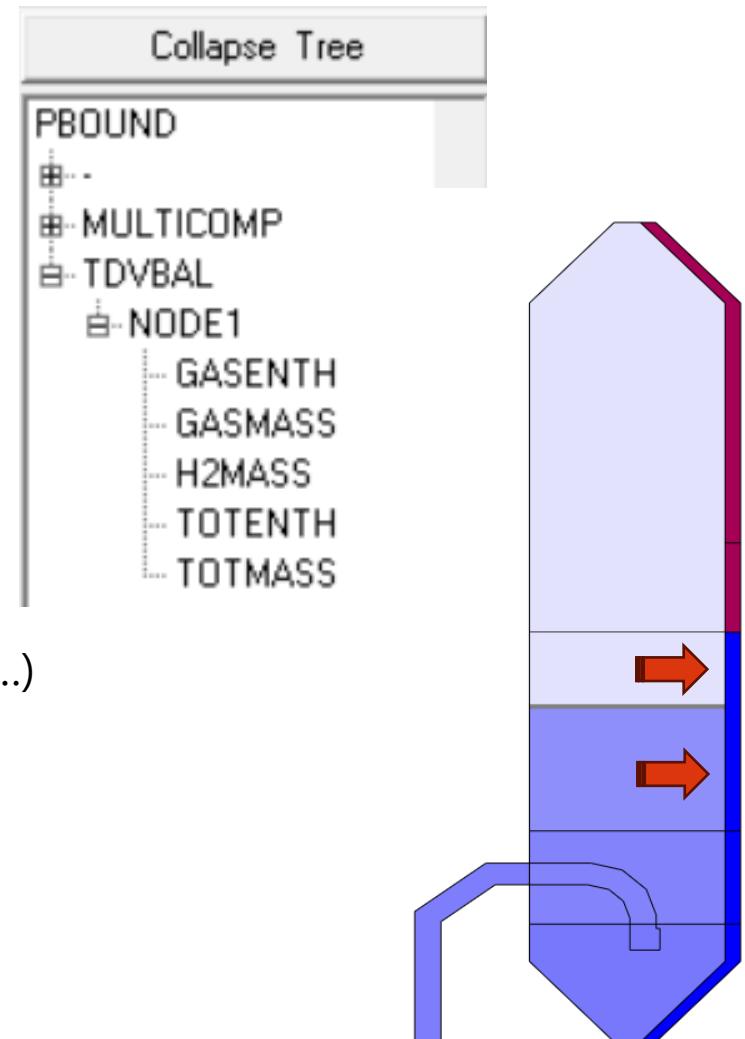
C---- PARAMETERS
CONFIG_1 = S*---
CONFIG_2 = S---
C---- TOPOLOGY
@      PRIORITY CHAINS
%CONFIG_1% COARSE
----- LOOP1
. . .
%CONFIG_2% FINE
----- LOOP1A
. . .
----- LOOP1B
. . .

```

S----	SPRAY	TEMPERATURE	X1NAME	X2NAME	X3NAME	X4NAME
@	YNAME	CONTYPE	TIME	-	TTSPRAY	-
@	STSPRAY	FUNGEN	A1	A2	A3	A4
	IOPT	GAIN	0.	0.	0.	0.

Additional Output Quantities

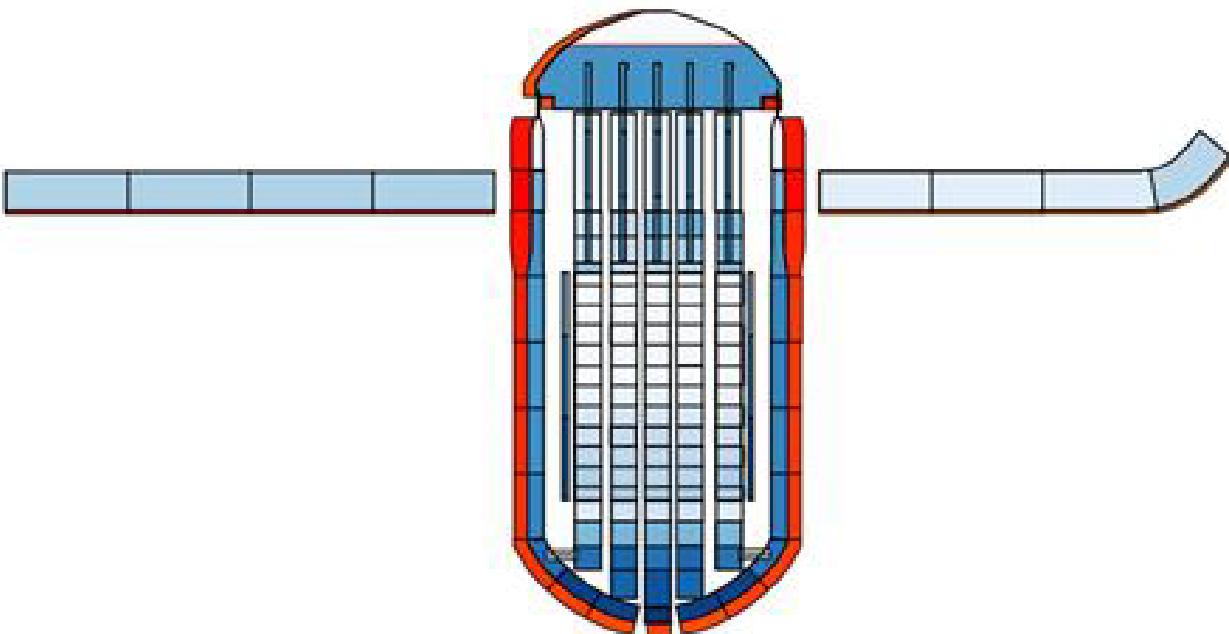
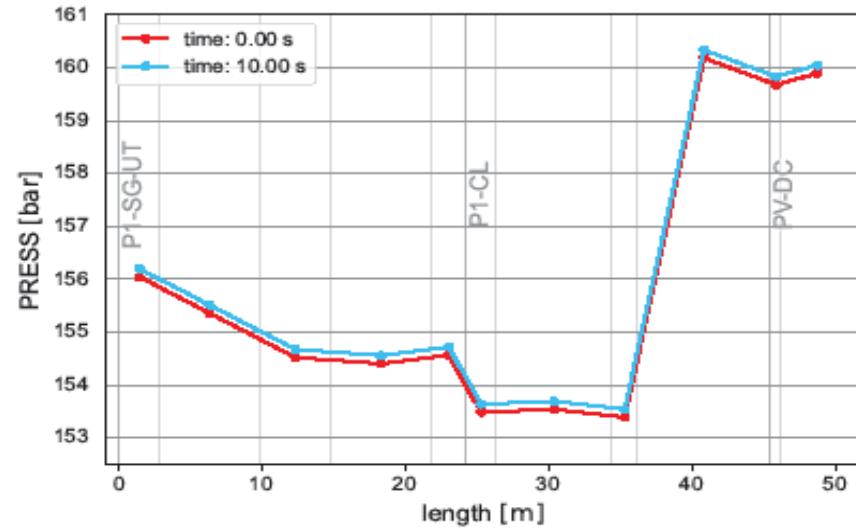
- **Integrated quantities for every TDV** (keyword TDVBAL)
 - Total (gas) mass and enthalpy flow towards/from the TDV
 - Mass flow per NC gas component
- Extended **balance quantities for TFD system** (TFDGENERAL)
 - Energy loss (ENLOSS): Integrated energy flow from TFD system into all connected HCOs except RODs and STEAMGENs
 - Total mass per NC gas component (e.g. NITMASS, OXYGENMASS,...)
- **HECU mixture level output under ML_LEFT or ML_RIGHT**
 - For mixture levels defined in TFOs on left/right side
 - Heat flows to sub-CVs QHLUP and QHLOW provided separately
 - Additional output for HTC, MODE, etc. for sub-CV above ML



ML_LEFT	I/J	IMLHL	INDHL	QHLUP	QHLOW	QLUP	QLLOW	HTCL	HTCVL	HTCOL	HTCMIL	MODEL
1	9	1		2.89E+06	7.18E+05	2.89E+06	7.18E+05	0.00E+00	0.00E+00	0.00E+00	4.39E+04	25

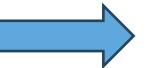
Batchplot Plotting Tool

- Python based plotting tool for hdf5 and pd data
- **Platform independent**, for Linux and MS Windows
- Plotting **temporal, axial and radial (HCO) distributions**
- **New module to visualize 2D graphics from AIG**
 - Dynamic visualization via Jupyter notebook possible
 - For details and examples see Batchplot manual



Summary

- **Numerous new and improved models in ATHLET 3.5**
 - Various new options for **detailed simulation of structures**, e.g. spacer grid model, 3D heat conduction, and new geometry type for horizontal plate
 - **New heat pipe module**, e.g. for investigation of **Micro Modular Reactors**
 - Improved modelling for **flow regimes and friction losses**
 - **User support and quality assurance** by extended input checks and output data
 - On-going integration of ATHLET and ATHLET-CD

 See **ATHLET Program Updates Manual** for complete listing

Thank you for your attention!

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**Gesellschaft für Anlagen- und
Reaktorsicherheit (GRS) gGmbH**
Schwertnergasse 1
50667 Köln



→ www.grs.de

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